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Accepted Manuscript

How to cite:

Science of The Total Environment. Volume 744, 20 November 2020, 140893.
<https://doi.org/10.1016/j.scitotenv.2020.140893>

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1 **Environmental assessment of complex wastewater valorisation by** 2 **polyhydroxyalkanoates production**

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6 **ABSTRACT**

7 Polyhydroxyalkanoates (PHA) are biodegradable polymers with renewable origin that
8 are expected to substitute conventional petrochemical plastics. However, before they are
9 commercialized, life-cycle environmental validation is needed, to prove that there is an actual
10 benefit with the replacement of non-renewable plastics with PHA. Nowadays, environmental
11 evaluations assessing bioplastics production at full-scale are scarce due to the lack of data, so
12 experimental results were used to evaluate the feasibility of PHA production employing high
13 load wastewater. A three-stage PHA production system utilising a mixed microbial culture
14 (MMC) was successfully operated for two years employing complex wastewater from a fish-
15 canning industry. The results obtained were scaled-up to define and compare a circular
16 economy scenario performance, with PHA production, with the current linear approach (i.e.
17 effluent generation, treatment and discharge). To the best of our knowledge, this is the first
18 time that the environmental performance of a MMC-based full-scale PHA production system
19 using saline wastewater is evaluated. Results show an average improvement of ca. 25 % for
20 nine out of ten studied categories if the circular economy approach is implemented. The sludge
21 management strategy was a key factor for the environmental validation of the process, and if
22 composting is applied instead of anaerobic digestion, the improvement is reported in eight
23 categories. When a more conservative replacement yield of fossil-based plastic was tested, the

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24 circular economy approach was the preferable option in 8 out of 10 categories. The significance
25 of the downstream process was also confirmed by this study, although it was not a barrier to
26 show the feasibility of producing added-value bioproducts under a circular economy approach.
27 Finally, this work proposes new process integration strategies to reduce the environmental
28 burdens of PHA production and increase the body of knowledge on MMC-based processes, an
29 area where LCA case studies are still scarce.

30 **Keywords:** Best available techniques; bioplastics; circular economy; industrial
31 wastewater; life cycle assessment; mixed microbial cultures

32 **Abbreviations**

AP	Acidification Potential
BAT	Best Available Techniques
CAS	Conventional Activated Sludge
COD	Chemical Oxygen Demand
DAF	Dissolved Air Flotation
DAR	Depletion of Abiotic Resources
DSP	Downstream Process
EP-F	Freshwater Eutrophication Potential
EP-M	Marine Eutrophication Potential
FBR	Fed-Batch Reactor
FU	Functional Unit
GWP	Global Warming Potential
HB	Hydroxybutyrate (monomer)
HRT	Hydraulic Retention Time
HT	Human Toxicity
HV	Hydroxyvalerate (monomer)
LCA	Life Cycle Assessment
LCI	Life Cycle Inventory
LCIA	Life Cycle Inventory Assessment
LLW	Low Load Wastewater
MCW	Mussels Cooking Wastewater
ME	Marine Ecotoxicity
MMC	Mixed Microbial Cultures
ODP	Ozone Depletion Potential
PET	Polyethylene Terephthalate
PHA	Polyhydroxyalkanoates
PHB	Polyhydroxybutyrate
POCP	Photochemical Oxidant Creation Potential

PP	Polypropylene
RR	Replacement Ratio
SBR	Sequencing Batch Reactor
SDS	Sodium Dodecyl Sulphate
SRT	Solids Retention Time
TAETP	Terrestrial Aquatic Ecotoxicity Potential
TSS	Total Suspended Solids
VSS	Volatile Suspended Solids
WWTP	Wastewater Treatment Plant

33

34 **1. Introduction**

35 Fish-canning industries play a significant role in the Spanish market, where the North-
 36 Western region of Galicia is the main mollusc producer of Europe (APROMAR, 2019). The
 37 production of mussels constitutes about the 80 % of the total Spanish fish-canning production,
 38 generating around 250 kt of mussels per year. This industry is an essential driving force for the
 39 region, since it is responsible for more than 100 M€ of annual income and for more than 10,000
 40 jobs, representing between the 15 % and 40 % of the total active population living in the areas
 41 in which mussels are harvested and processed (Rey-Méndez et al., 2016).

42 However, the fish-canning industry activity generates high amounts of complex
 43 wastewater containing salts, organic matter, nutrients and solids, among other compounds.
 44 Moreover, the wastewater coming from the boiling of mussels (or mussels cooking wastewater,
 45 MCW) is a highly polluted effluent which treatment is challenging. In fact, the environmental
 46 concern regarding the treatment and disposal of MCW is high, and several measures (economic
 47 incentives, research projects, environmental policies...) were applied to solve the issue related
 48 to MCW, as reflected in specific legislation (Consellería de Medio Rural e Mar, 2015). These
 49 effluents constitute a threat for the industry, which is obviously dependent on the water quality
 50 of the areas where seafood is harvested. These areas, called *rías* or estuaries, are unique spaces
 51 with a high biological diversity, optimal for the farming and growth of seafood. Therefore, it

52 is important to treat properly those industrial effluents to guarantee the environmental stability
53 of the estuaries and the economic sustainability of this region.

54 Although the presence of salts, sulphate and other compounds which are characteristic
55 of fish-canning effluents can hinder or inhibit biological activity, biological treatments (like
56 activated sludge or anaerobic digestion) were possible in the past when specific operational
57 strategies were applied (Palmeiro-Sánchez et al., 2013). Considering this, it is of interest to
58 explore alternative routes for the biological treatment of these high-salinity wastewaters, and
59 for their valorisation under the circular economy perspective.

60 Polyhydroxyalkanoates (PHA) are polyesters produced as intracellular storage
61 materials by a wide range of microorganisms. The characteristic that makes these biopolymers
62 an interesting alternative to conventional plastic is that they combine high functionality with
63 biodegradability and non-toxicity. Due to the microbial origin of PHA, 40 – 48 % of the total
64 production costs are related to the employed feedstock (Rodríguez-Perez et al., 2018), while
65 the remaining costs correspond to the energy employed to maintain sterile conditions for the
66 microorganisms culture, and the downstream process (DSP) for PHA extraction (Fernández-
67 Dacosta et al., 2015). The use of waste streams, such as industrial wastewater, and non-sterile
68 mixed microbial cultures (MMC) would not only reduce the cost of the final product, but also
69 improve the environmental performance of the process (Yadav et al., 2020). Furthermore, the
70 research for new materials that can substitute conventional plastics is essential for
71 accomplishing the ambitious objectives targeted by the European Commission (European
72 Commission, 2018). Moreover, the production of bioplastics employing wastewater is of great
73 interest, especially in coastal areas, because of the link between plastic pollution and the

74 destruction of the marine ecosystems, which directly impact not only the environment, but also
75 the local economy (Conejo-Watt and Luisetti, 2019)².

76 In this scenario, TREASURE-TECHNOSALT project³ aims to unravel the effects of
77 salinity over biological processes in wastewater treatment and valorisation, and biopolymer
78 production is being technologically assessed under high salinity conditions. However, the
79 aspects that need to be considered for biopolymer commercialization are not only related to
80 technical issues but also to environmental concerns. Conventional plastics, which constitute a
81 serious problem for ecosystems and human health worldwide, are dependent on oil and petrol.
82 Therefore, new sources for plastic production are being researched and it is necessary to prove
83 the environmental benefits of those novel alternatives compared to the non-renewable ones and
84 to establish criteria for their applications and safe disposal (European Commission, 2018). In
85 this context, Life Cycle Assessment (LCA) seems to be the appropriate tool, since it has already
86 been widely used to assess the environmental performance of different processes and products,
87 and particularly of PHA production processes (Bengtsson et al., 2017; Fernández-Dacosta et
88 al., 2015; Morgan-Sagastume et al., 2016). However, recent investigations pointed out the
89 urgent need for studies in which all process stages are covered, establishing PHA biosynthesis
90 and extraction from waste as feedstock. This lack of research works in which the whole process
91 is holistically studied is drawing back the scale up and commercialization of PHA (Mannina et
92 al., 2020).

93 The objective of this study is then to evaluate the environmental performance of a PHA
94 production process from high salinity wastewater using MMC and to compare it with the
95 traditional linear economy approach (i.e. wastewater treatment and discharge). All process
96 stages, from waste generation to product extraction and effluent discharge will be evaluated.

² <http://www.cleanatlantic.eu/>

³ <http://www.usc.es/biogroup/treasure>

97 Therefore, the new data provided will contribute to increase the information available on full-
98 scale MMC-based PHA production systems. To do so, lab activities carried out within the
99 TREASURE-TECHNOSALT project will be used for the scaling-up of the process and
100 complemented with literature sources when needed, and the environmental impacts of PHA
101 production will be quantified. Here, a MMC-based PHA production process employing saline
102 wastewater will be environmentally assessed for the first time.

103 **2. Goal and scope definition**

104 The goal of this study is to evaluate the use of high salinity wastewater as a feedstock
105 for PHA production. To do so, a PHA production system at lab-scale was operated using MCW
106 coming from a local industry where molluscs were boiled.

107 However, the production of PHA from wastes using MMC is still under development,
108 with only a few pilot-scale plants operating worldwide (Kourmentza et al., 2017). In this
109 scenario, the environmental evaluation of the process is challenging, since LCA results using
110 lab-scale data do not necessarily represent the impacts associated to a full-scale process, often
111 resulting in an overestimation of the outcomes (Moni et al., 2020). To minimise that, the present
112 LCA is based on an up-scaling of the system from the results obtained at laboratory-scale (18
113 months of stable operation), where different operational conditions were tested and optimized
114 (Roibás-Rozas et al., Unpublished Results).

115 **2.1 Functional Unit (FU) definition and feedstock quantification**

116 The functional unit (FU) is usually defined in terms of the system output, and this has
117 been the case for PHA production system, in which the FU defined is normally related to the
118 mass of biopolymer generated, being 1 kg or 1 t of PHA (or specifically polyhydroxybutyrate,
119 PHB) the preferred option (Zarrolì, 2020). Having said that, literature states that the minimum
120 amount of biopolymer needed to make a MMC-PHA production process economically feasible

121 is around 10^3 t PHA/year (Bengtsson et al., 2017). With the chosen substrate, MCW, and
122 system productivity (see below), the amount of wastewater needed to guarantee the economic
123 feasibility of the process would be approximately $1,500 \text{ m}^3/\text{day}$, which is a high and unrealistic
124 flow considering the processing capacity of the region. In fact, when dealing with waste
125 management systems, the FU might be defined in terms of the system input, that is the waste
126 to be managed. This has been the approach taken by recent studies on PHA production when
127 the feedstock employed was wastewater: an influent volumetric-based FU, such as the
128 treatment of a certain amount of wastewater flow rate (Morgan-Sagastume et al., 2016). This
129 approach might be questionable when different wastewater streams are compared, since it
130 disregards their loads and characteristics, but not in the case where two scenarios, i.e. linear
131 and circular economy based, are compared for the same type of wastewater as occurs in the
132 present study. As a result, this second approach, the system input FU, is the one selected here
133 and its quantification is described next.

134 As already stated, Galicia produces annually about 250 kt of mussels, of which about a
135 40 % is consumed fresh and the 60 % remaining is processed (i.e. boiled and canned).
136 Furthermore, almost 70 % of the mussel rafts are located in the area of *Arousa* (Barros et al.,
137 2009). Currently, there are ten facilities allowed to boil mussels in Galicia, nine of them in
138 *Arousa* (Consello Regulador do Mexillón de Galicia, 2020). Consequently, it can be assumed
139 that the mussel processing in Galicia takes place in this estuary. Among those nine, the three
140 biggest ones are responsible for the processing of about 45 kt of mussels/year each (Mejillones
141 Nidal, 2018), so this study focuses on these three plants (Figure 1). As the distance among
142 boiling facilities is shorter than 10 km, it is justified to evaluate a centralized wastewater
143 valorisation and treatment plant for a full-scale PHA production scenario.

144 FIGURE 1 AROUND HERE

145 The processing of mussels usually generates two kinds of effluents that are treated
146 separately in the processing facility before they are discharged (Barros et al., 2009): a low-
147 loaded wastewater stream (LLW), mainly resulting from washing operations, and a high-loaded
148 one, from the boiling of the molluscs. The LLW only needs basic primary treatment, such as
149 screening, before safe discharge. It is always produced, and it is out of the scope of this study.
150 The high-loaded one, the MCW, is our target effluent due to its high carbon content and to its
151 treatment complexity. This stream has a highly variable composition, which average values are
152 reported in Table 1.

153 TABLE 1 AROUND HERE

154 Regarding wastewater production, a processing facility of high capacity generates
155 about 5 m³/t of mussels processed, of which a 6 % is considered of high load (Bello Bugallo et
156 al., 2012). As 100 - 105 kt of mussels are assumed to be processed by the three facilities per
157 year, the centralized full-scale plant for the valorisation and treatment of MCW would have an
158 input flow of 85 m³/day, considering 365 working days per year (Secretaría xeral de Calidade
159 de Avaliación Ambiental, 2013a)⁴. This is a value significantly lower than the threshold level
160 reported above for economic feasibility. Nevertheless, and considering the expected evolution
161 of this novel technologies, this flow is chosen as the FU for this study, as it is the available
162 flow of the researched feedstock in the target area. This centralized scenario will be compared
163 with the current one, in which MCW is treated in the industrial wastewater treatment plant
164 (WWTP) of each processing facility before being released. When the fish-canning facility is
165 located in an industrial area, the effluents are usually disposed to the sanitation network with
166 low requirements regarding discharge limits (Dirección Xeral de Calidade e Avaliación
167 Ambiental, 2008a). One of the problems linked to mussels processing industry is that facilities

⁴ The feedstock quantification is based on an annual production so the number of working days will neither change the annual wastewater generated or the total PHA production.

168 are usually located in coastal areas, away from industrial zones. Therefore, after wastewater
169 treatment, the effluent is usually disposed directly into the estuaries through a sewage pipe,
170 with variable discharge limits.

171 **2.2 System boundaries and scenarios definition**

172 The system starts with the MCW generation, so the upstream processes, i.e. the
173 harvesting and canning of the molluscs, are left out the system boundaries. Besides, the
174 treatment and discharge of LLW is also left out as it is a common process for all the scenarios
175 under evaluation. The system boundaries of the present study include all the processes involved
176 in wastewater treatment and valorisation: water line from the influent pumping to the final
177 discharge of the effluent in the receiving water body, sludge management and disposal, and
178 bioplastic production (extraction of the PHA from the biomass).

179 Sludge is produced from the MCW treatment and valorisation processes and, according
180 to the Spanish legislation, biowaste has to be treated through anaerobic digestion or
181 composting, encouraging administrations to promote the use of the resulting organic fertilizers
182 in agriculture (Jefatura del Estado, 2011). A total of 19 facilities in Galicia are authorised for
183 sludge valorisation, and only three of them work with anaerobic digestion, while the rest of
184 them are mainly compost producers (Xunta de Galicia, 2020). Therefore, transport to the
185 nearest of these facilities and sludge composting is considered for the conventional scenario,
186 while anaerobic digestion at the centralized facility for the valorisation scenario is considered
187 as the most feasible choice. However, due to the lack of information concerning the sludge
188 characteristics, the final application of the compost and the digestate are excluded from the
189 evaluation.

190 For all the stages, only the environmental impacts associated with operation have been
191 considered in the study, while construction and decommissioning of the required
192 infrastructures have been excluded due to lack of data.

193 **2.2.1 Baseline scenario: the LINEAR ECONOMY approach**

194 High strength fish-canning wastewater (like MCW) is usually treated in two stages:
195 primary and secondary. In primary treatments, solids and oily matter are removed from the
196 wastewater, while, in the secondary one, biological systems are usually employed to remove
197 dissolved organic matter and nutrients. The choice of the best available technique (BAT)
198 ensures the minimum environmental impact without compromising the economic performance
199 of an installation. BAT selection, which is based on technical feasibility, environmental
200 benefits and economic profitability, establishes the following treatment sequence for fish-
201 canning effluent: first, a primary treatment (equalization, screening, sedimentation, pH
202 adjustment, flocculation, flotation, or microfiltration) and then, a secondary treatment (aerobic
203 or anaerobic). Therefore, the up-scaling of the linear economy scenario will be based on the
204 treatments recommended in the BAT for fish processing (Tomczak-Wandzel et al., 2015), as it
205 is commonly the base for WWTP design in MCW treatment (Mejillones Ría de Arosa, 2016).

206 For primary treatment, the use of Dissolved Air flotation systems (DAF) is widely
207 spread due to their high efficiency and simplicity, and they are used to treat MCW (Barros et
208 al., 2009). When coagulants are employed, its removal efficiency increases to 80 – 95 %, since
209 the DAF unit will be able to separate not only solids, but also soluble organic compounds that
210 can precipitate and be removed (Tomczak-Wandzel et al., 2015). In the fish-canning industry,
211 it is recommended to operate at a pH approximately of 5 in order to decrease protein solubility.
212 As MCW have high protein concentration, the use of this unit is justified (Figure 2), and its
213 aim is to remove not only solids, but also organic nitrogen associated to proteins.

214 **FIGURE 2 AROUND HERE**

215 Concerning secondary treatment, biological processes are the preferred option
216 (activated sludge, anaerobic digestion, granular treatments, etc.). Anaerobic digestion has been
217 employed, but the experience has only been fully successful in facilities with low salinity

218 wastewater (Secretaría xeral de Calidade de Avaliación Ambiental, 2013b), as the presence of
219 sodium, ammonia and sulphate can hinder anaerobic treatments. For MCW, these ions are
220 normally present in inhibitory concentrations, and methane production is very difficult. Despite
221 this fact, several full-scale experiences were carried out in the past in Galician industries trying
222 to valorise MCW anaerobically, but with unsuccessful results where the low amounts of poor
223 quality biogas produced were permanently burned in a torch (Barros et al., 2009). Therefore,
224 most of the industrial plants for fish-canning processing employ activated sludge processes for
225 the wastewater secondary treatment, as it is the conventional treatment defined here. Each
226 canning facility is supposed to have a small WWTP for the treatment of their effluents (Figure
227 2); so, assuming equal production capacities, the capacity of each WWTP for the linear
228 economy scenario is supposed to be 1/3 of the total MCW generation, i.e. 28.3 m³/day.

229 Sludge is thickened and stored in an industrial container. Once the container is full, it
230 is transported to the closest industrial composting facility.

231 **2.2.2 CIRCULAR ECONOMY approach**

232 The valorisation scenario was designed from the knowledge acquired in previous
233 research projects (see section 1 of the Supplementary Material (SM)) and the experimental
234 results after two years operating a bench-scale three-stage system for PHA production
235 employing MCW (Figure 3). For more information about the lab-scale three-stage system for
236 PHA production, see section 2 of the SM. First, in the acidification stage, Chemical Oxygen
237 Demand (COD) present in the MCW is transformed into Volatile Fatty Acids (VFA). The
238 acidification reactor and its start-up is described in Fra-Vázquez et al.(2020). After biomass
239 separation by centrifugation, VFA are fed to two reactors: a Sequencing Batch Reactor (SBR)
240 and a Fed Batch Reactor (FBR). The SBR is an enrichment reactor for the MMC selection,
241 while the FBR is employed to maximize PHA content in the MMC. Several operational
242 strategies were tested throughout the experimental time (Roibás-Rozas et al., Unpublished

243 Results). Optimal conditions were found when a mild alkalinity addition was performed by the
244 supplementation of 80 mg Na(HCO₃)/L to the MCW fed to the acidogenic reactor. The
245 enrichment reactor operated with Modified Aerobic Dynamic Feeding, in which Feast-Famine
246 regime was combined with a settling stage as explained by Argiz et al. (2020), who operated a
247 reactor with the same inoculum as the one described here.

248 FIGURE 3 AROUND HERE

249 Biological nitrification was inhibited in the SBR by allylthiourea addition (20 mg/L of
250 feeding). When its addition was stopped, this biomass was able to produce nitrite during the
251 famine period, with a nitrification rate of 30 mg NH₄⁺-N consumed/g Volatile Suspended
252 Solids·d (NH₄⁺-N/(g VSS·d)). Denitrification occurred during the anoxic periods of feast, where
253 all nitrite was consumed with no significant worsening of the enrichment performance (Fra-
254 Vázquez et al., 2019).

255 In addition to the desired stream, the PHA-rich one, other streams are produced. They
256 are unified in a single stream to be treated together and safely released to the environment.
257 Therefore, a primary settler is required to remove solids present in this waste stream and to
258 work as an homogenization unit to change from sequential operation to a continuous mode.
259 Then, a biological treatment will be employed to remove nitrogen and organic matter in a
260 conventional activated sludge system (CAS), in which aerobic nitrification and anoxic
261 denitrification are performed in a step-fed type system with four anoxic/aerobic sections.
262 Sludge generated in every stage of the process is treated anaerobically in a sludge digester.

263 The experiences carried out at lab-scale comprise only the valorisation steps, in which
264 an effluent is generated for treatment and disposal, and PHA-rich biomass is produced for
265 extraction. Therefore, experimental data developed in the frame of TREASURE-
266 TECHNOSALT were employed for the up-scaling of the biological valorisation line. For the

267 extraction and refining stage (i.e. DSP), data from USABLE PACKAGING project⁵ were used.
268 Environmental and techno-economic analysis showed that purification of PHA employing
269 alkaline treatment with sodium dodecyl sulphate (SDS) is a promising choice for PHA
270 extraction from MMC (Saavedra del Oso, 2020), so data from the provided inventories are used
271 in the present study. For the selected treatment (SDS and sodium hypochlorite), 99.9 % purity
272 was established according to Fernández-Dacosta et al. (2015) and an ideal recovery yield was
273 assumed (discussed later on, see section 5.3).

274 Concerning the avoided product, PHA properties showed similar specifications to
275 poly(ethylene terephthalate) (PET), poly(ethylene), poly(styrene) and poly(propylene) (PP)
276 (Koller et al., 2013). PP is similar to PHB polymers, although when other monomers are
277 included in the chain, like hydroxyvalerate (HV), plastic properties change (Palmeiro-Sánchez
278 et al., 2016). Biopolymer composition in TREASURE-TECHNOSALT project was
279 approximately 25:75 HV:HB. Recent studies show that this type of biopolymer could substitute
280 PET for packaging applications (Melendez-Rodriguez et al., 2018) so PET is the conventional
281 plastic selected as avoided product from the PHA production. Note that neither the use nor the
282 end-of-life stages for both conventional and bio-based plastics are included in the present study.

283 Finally, the design of the anaerobic reactor for the sludge valorisation was performed
284 according to the results obtained in the frame of PLASTICWATER⁶ project, where the
285 anaerobic digestion of sludge under brackish conditions and high ammonia and sulphate
286 concentrations was successfully assessed (Palmeiro-Sánchez et al., 2013).

287 **2.2.3 Mass balances and stream compositions**

⁵ <https://www.bbi-europe.eu/projects/usable-packaging>

⁶ Recycling of wastewater and sludge to produce bioplastic materials (PLASTICWATER). Supported by Spanish Government (CTQ2011-22675)

288 Table 2 summarizes the composition of the main streams of every scenario and
289 compares the achieved effluent with the discharge limits. As there is few information available
290 regarding these limits in mussels boiling facilities, they were established according to the
291 specifications imposed on a fish-canning company discharging its effluent directly to the
292 *Arousa* estuary or *ría de Arousa* (Dirección Xeral de Calidade e Avaliación Ambiental, 2008b),
293 which is the area where the majority of the mussels boiling facilities are located (Fig 1). More
294 information about the design of every process unit and the mass balances performed is supplied
295 in section 3 of SM.

296 TABLE 2 AROUND HERE

297 **2.3 Life Cycle Impact Assessment: impact categories and method selection**

298 The choice of the relevant impact categories and impact assessment methodology is
299 essential to provide a consistent evaluation of the environmental performance of the scenarios
300 under study. As this research has a circular economy approach, several review papers and
301 articles were examined in order to identify the most common impact categories assessed in the
302 different areas covered by this study: WWTP operation and management, plastic
303 production/waste and PHA production. Here, the lack of studies regarding MMC-based PHA
304 production is noticeable, and most research works focus on pure culture processes. Table 3
305 shows the result of this review. All of them will be covered in this study, paying special
306 attention to the four first ones. For eutrophication, both freshwater and marine will be assessed
307 (EP-F and EP-M, respectively). Besides, and considering the particularities of this study,
308 Marine Ecotoxicity (ME) will also be considered.

309 TABLE 3 AROUND HERE

310 The Hierarchist ReCiPe 2016 Midpoint method (v1.13) has been selected to evaluate
311 all the selected impact categories except Global Warming Potential (GWP), which was

312 assessed by the last update of the IPCC method (v 1.03 100a). SimaPro v8.3 was used for the
313 computational implementation of all the inventories and impact categories calculations.

314 **3. Life Cycle Inventory**

315 Mass balances were employed to estimate the composition and flows of every stream
316 (section 2.2.3) and complemented with literature data when needed. Conventional treatment
317 units were designed following wastewater treatment and chemical engineering handbooks
318 (Coulson and Richardson, 1999; Metcalf & Eddy, 2014). Theoretical power equations
319 (described in the section 3.3 of the SM) were used to determine the energy requirements of
320 every stirrer, blower, centrifuge and pump. Chemicals dosage was estimated using laboratory
321 results and literature data. Results of all the calculations are summarised in Table 4, and
322 detailed information is given below.

323 TABLE 4 AROUND HERE

324 **3.1 Inventory of the linear economy scenario**

325 As already stated, three facilities were considered for boiling mussels. Therefore, the
326 design was individually performed considering a third of the total flux. Then, the linear
327 economy scenario was built up putting together the three facilities.

328 - Design of the process units:

329 The DAF unit removes 85 % of solids and, with the use of coagulants at low pH, about
330 40 % of the COD. A volume of 1 L HCl per m³ of wastewater is assumed to be added to lower
331 pH to 5 (and equimolar amounts of NaOH are supplied after DAF to raise pH to neutrality).
332 The removed COD is 80 % of coagulated proteins, eliminating approximately a 35 % of total
333 nitrogen, and approximately 30 % of carbohydrates. After DAF unit, COD/N ratio in the
334 wastewater is high (approximately 12), so two aerobic ponds are employed to ensure the

335 removal of organic matter, while nitrogen is supposed to be consumed mainly due to cell
336 growth. Mass balances were performed to determine Solids Retention Time and Hydraulic
337 Retention Time (SRT and HRT, respectively) and the number of ponds needed to achieve
338 discharge limits. Short SRT (5 days) guarantees avoiding nitrification in the first pond, so
339 ammonia and COD consumption is calculated by mass balances according to the SRT. A
340 second pond with extended aeration (SRT = 40 days) is needed to achieve COD levels
341 according to legal requirements considering the available ammonia. Due to the long SRT in
342 the second pond, some ammonia oxidation can take place, and it was estimated from mass
343 balances (see Table 2).

344 - Direct emissions to air:

345 Biogenic CO₂ emissions related to COD consumption were calculated based on the
346 emission factor reported by Campos et al. (2016): 0.08 kg CO₂/kg COD consumed. As COD/N
347 ratio after DAF is about 12, nitrogen is consumed for biomass assimilation with no nitrification.
348 According to the latest IPCC update for greenhouse inventories (IPCC, 2019), N₂O emissions
349 are generally expected for aerobic systems. Depending on the stream characteristics and
350 treatment system employed, they can vary from negligible to significant, with a emission factor
351 range of 0.00016-0.045 kg N₂O-N/kg N in influent. In the linear economy scenario, as the main
352 consumption of ammonia is related to cell growth, a low emission factor of 0.012 kg N₂O-N/kg
353 N is chosen.

354 - Sludge production and management:

355 Sludge generated in DAF units usually has 4 % of solids concentration (Metcalf &
356 Eddy, 2014). With 85 % solids removal efficiency, sludge generation is 1.8 m³/day. Secondary
357 sludge production was calculated according to SRT and decanters performance, producing 7.7
358 m³/day of sludge with 7.43 g VSS/L. Sludge is thickened in a gravity thickener to reach a

359 concentration of 45 g Total Suspended Solids/L (g TSS/L) (Metcalf & Eddy, 2014) and then
360 transported to external facilities for further management. Chemically clarified supernatant is
361 mixed with LLW, and as its contribution is less than 1.5 % of its flow (6.33 versus 430 m³/day),
362 the influence of this stream on the LLW treatment can be disregarded. After that, sludge is
363 composted together with other waste streams (41 % average of sewage sludge as feedstock
364 (TEN, 2020) was considered).

365 **3.2 Inventory of the circular economy scenario**

366 The centralised scenario that treats the total MCW flow (section 2.1) was up-scaled
367 from the data obtained in the lab. Theoretical equations were used to calculate power needs,
368 the operating time of the equipment, etc (see section 3 of the SM).

369 - Design of the process units:

370 In the valorisation line, the up-scaling was performed considering the obtained results.
371 The effluent of the acidification reactor, which operated at SRT = HRT of 6.5 days, had 0.6 g
372 COD_{VFA}/g COD. The SBR consumed 1.21 g COD_{VFA}/g biomass to reach 4 g VSS/L, and FBR
373 needed 2.98 g COD_{VFA}/g biomass to achieve 41.5 % accumulation capacity. Overall, process
374 efficiency was of 0.2 kg COD_{PHA}/kg COD_{MCW}. In the treatment line, to ensure nitrifiers growth,
375 SRT in the step-fed CAS was set at 15 days and HRT in the anoxic volume was 58.83 m³.
376 Antifoaming agent (0.5 mL triethylene glycol/L feeding) was supplied in the SBR and NaOH
377 was used for pH adjustment in the SBR and FBR (0.75 and 1 g NaOH/L, respectively), based
378 on laboratory-scale dosages.

379 - Direct emissions to air:

380 Direct emissions of the acidogenic unit were estimated from lab measurements and
381 literature data. Waste mixtures containing carbohydrates and proteins in acidogenic fermenters
382 generated about 279 mL biogas/g VSS, with 47 % of CO₂ (Alibardi and Cossu, 2016). No

383 methane was detected in several years of operation, and 2.4 % of the reactor headspace was
384 H₂S as a consequence of the high sulphate concentrations in MCW. For this reason, ferrous
385 oxide pellets, which are by-products of metallurgic industry, are used to remove H₂S with a
386 ratio of 0.6 g H₂S/g pellet (Allegue and Hinge, 2014). When pellets cannot be used anymore,
387 they are employed as raw material for roads and bricks. Fossil CO₂ is produced due to alkalinity
388 addition, and CO₂ emissions were calculated for operational temperature and pH. For the
389 aerobic reactors of the valorisation line, biogenic CO₂ generation due to COD consumption is
390 0.08 kg CO₂/kg COD (Campos et al., 2016) and due to PHA generation is 30 % (C-mol PHA/C-
391 mol CO₂) (Jiang et al., 2011).

392 Regarding N₂O emissions, as nitrification and denitrification take place in the circular
393 economy scenario, more N₂O is supposed to be generated. According to the latest IPCC update
394 for greenhouse gas emissions (IPCC, 2019), the average value for the emission factor is 0.016
395 kg N₂O-N/kg N in influent for aerobic systems (as emissions for anaerobic units are not
396 expected). This factor will be considered for the circular economy approach, assuming that
397 nitrogen removal takes place not only in the anoxic tank of CAS but also during SBR feast.

398 - Sludge production and management:

399 Sludge is produced in the centrifuge after the acidification unit, in which most of the
400 solids are removed and 1 m³/day of sludge with 25 % TSS is generated (Elías, 2012). Primary
401 settler after the valorisation line removes 55.75 % of solids and 33.96 % of COD, according to
402 theoretical equations (Metcalf & Eddy, 2014), and produces 1.3 m³/day of sludge with 5 %
403 TSS. CAS unit generates sludge according to SRT and decanter performance, producing 4.0
404 m³/day with 6.90 kg VSS/m³, which is thickened in a gravity thickener to reach a final
405 concentration of 45 g TSS/L (Metcalf & Eddy, 2014). The clarified stream from the thickener

406 is diluted and treated together with the LLW⁷, and the concentrated stream is treated together
407 with the other high-solid streams in an anaerobic digester.

408 Regarding biogas production, sludge valorisation under high concentrations of sodium,
409 sulphate and ammonia is feasible after proper biomass acclimation and process control.
410 Moreover, sludge digestion generated 280 L of biogas/kg VSS (with 58 % of methane) when
411 the digester feeding composition contained 6.7 g Na⁺/L and 1.5 g SO₄²⁻/L (Palmeiro-Sánchez
412 et al., 2013). As these conditions are similar to the ones that could be found in this digester, the
413 obtained results will be employed for the design of the digestion unit. Finally, biogas
414 valorisation is performed considering electric and heat efficiencies of 35 % and 45 %,
415 respectively (Metcalf & Eddy, 2014): i.e. 133.9 kWh/day of heat energy and 104.2 kWh/day
416 of electricity. The former was used to maintain the temperature of the digester at 38 °C and the
417 latter was sent to the grid and considered then as avoided product. An amount of 1.5 % of the
418 produced biogas is leaked, while the presence of N₂, H₂S and NH₃ in the biogas is estimated in
419 1 %, 0.05 % and 0.01 %, respectively (Rodriguez-Verde et al., 2014). Emissions linked to
420 biogas combustion are calculated from literature data (Paolini et al., 2018), and ferrous oxide
421 pellets are employed for sulphide removal before valorisation.

422 - Downstream Process:

423 DSP design is indicated in Fernández-Dacosta et al., 2015 (surfactant-hypochlorite
424 method). Wastewater generated in DSP is diluted with LLW for its safe disposal (contribution
425 of less than 0.5 % in volume) and therefore left out the system boundaries⁸.

426 - Energy integration:

⁷ As the supernatant only represent less than 0.5% of the LLW flow (5.64 m³ versus 1290 m³), this addition is considered negligible and stays out the system boundaries.

⁸ Same criteria than the one applied for the supernatant of thickener, with a DSP wastewater flow of 3.02 m³/day

427 Following a circular economy approach, energy integration is also applied. The
428 temperature of MCW leaving the boilers is 125 °C, and the bioreactors in the valorisation line
429 operate at 38 °C and 30 °C, for the acidogenic reactor and the SBR-FBR respectively. Currently,
430 this heat is dissipated naturally in the facilities, so an estimation of the available heat was done
431 (1,000 kWh/day). It can cover the heat requirements of the biological reactors (estimated to be
432 around 500 kWh/day) as well as the heat demand of the DSP (about 100 kWh/day). Therefore,
433 the heat contained in MCW after the boilers is enough to cover the heat used in the process
434 units.

435 **3.3 Background processes**

436 Data for the processes of the background system (production of electricity, chemicals,
437 transport, plastic materials, steam and composting process) come from the Ecoinvent v3.3
438 database (Weidema et al., 2013). The Spanish electricity mix has been adapted with the most
439 recent update reported, referred to 2018 (Red Eléctrica Española, 2019). No environmental
440 burdens are allocated to the antifoaming agent (triethylen glycol) as it is a by-product of
441 ethylene oxidation, neither to the ferrous oxide pellets as they are considered waste from the
442 metallurgic industry. Therefore, only the transport of these products is considered. In the case
443 of ferrous oxide, as it is employed as a component in the production of roads and asphalt,
444 transport to the recycling facility (asphalt producer) is also included. As the SDS used at the
445 DSP is not available in the database, its background production process has been assimilated
446 to the one of alkylbenzene sulfonate.

447 **4 Life Cycle Impact Assessment**

448 **4.1 Individual environmental performance of each scenario**

449 The contribution of the different elements to the set of impact categories for each
450 scenario is presented in Figure 4.

451 FIGURE 4 AROUND HERE

452 For the linear economy scenario (Fig 4a), electricity has an important contribution for
453 all the categories (between 12 – 68 %) except for EP-M. Besides, chemicals consumption
454 (which also includes the transport from the suppliers) also has a relevant impact (13 – 87 %,
455 except for EP-M), mainly due to hydrochloric acid production. This process affects HT,
456 TAETP and ME, and direct emissions of chlorine impact on GWP. Composting (sludge
457 management) process has significant effects on GWP, AP and POCP due to the expected
458 emissions of CH₄, NH₃ and N₂O.

459 Behind the direct emissions label, direct emissions to air estimated in each scenario and
460 the release to the ocean of the final effluents are included. Regarding the former, direct
461 emissions to air also contribute to the GWP category in both scenarios, totally dominated by
462 the N₂O release. Concerning the latter, the release of an effluent containing nitrogen (in the
463 forms of ammonia and nitrate) is clearly impacting EP-M category for both scenarios. In the
464 linear economy scenario, no nitrification is expected, but small amounts of nitrate can be
465 produced in the second pond (SRT = 40 d and low COD concentration). Total nitrogen released
466 is 23.5 mg N_T/L, which is mainly ammonia nitrogen (15.0 mg NH₄⁺-N/L and 8.47 mg NO₃⁻-
467 N/L). For the circular economy scenario, nitrification and denitrification are needed as further
468 treatment to guarantee the discharge limits accomplishment, and the total nitrogen in the
469 effluent is 18.0 mg N_T/L, distributed between ammonia (4.0 mg NH₄⁺-N/L) and nitrate (14.0
470 mg NO₃⁻-N/L). Nevertheless, the implementation of innovative process approaches, like
471 nitrogen removal by the anammox process or phosphorous recovery units, could not only
472 mitigate negative effects in EP-M category, but also decrease the overall process impacts due
473 to energy optimization, better effluent quality and substitution of chemical fertilizers (Morgan-
474 Sagastume et al., 2016).

475 When looking at the circular economy scenario (Fig 4b), the environmental burdens are
476 more evenly distributed among the different elements, and electricity, chemicals use, and DSP
477 are the main contributors for most categories. The centralized characteristics of this plant,
478 which imply the transport of the MCW by lorry to the valorisation plant (i.e. labelled transport
479 at Fig.4b), have a non-negligible contribution in TAETP, HT and ME due to non-exhaust
480 gasses emissions linked to the brake wear treatment, and containing several harmful particulate
481 matter (like copper or antimony).

482 The environmental benefits related to the circular economy approach are dominated by
483 the avoided production of plastic (i.e. PET). The most affected category is fossil depletion
484 (DAR) (32 %), as the use of crude oil and natural gas is prevented. It also has non-minor
485 benefits for many other impact categories, like POCP, AP or ME, mainly due to the avoidance
486 of xylene formation. The energy recovered for electricity production and sent to grid also has
487 a net credit (net negative values for sludge management at Fig 4b), although with small values
488 due to the low load entering the digester (as most carbon in MCW is employed for PHA
489 valorisation) and the resulting low biogas production per m³ of MCW.

490 **4.2 Comparison of scenarios**

491 Figure 5 shows the comparative environmental analysis of the evaluated scenarios
492 (absolute values per category are reported in SM, Section 4, Tables S3 and S4). The current
493 linear economy approach shows the worst performance for all the impact categories evaluated,
494 except for ozone depletion potential (ODP), reporting an average improvement of 24.8 % when
495 a strategy of valorisation of the wastewater as the circular economy scenario described in the
496 present research work is applied.

497 FIGURE 5 AROUND HERE

498 The DSP is behind the worse performance of the circular economy scenario for ODP
499 due to the chemical intensity of that stage (in particular the hypochlorite production is the main
500 contributor for this category). Additionally, the use of sodium hydroxide for pH control in this
501 scenario has also negative effects on ODP. Possible improvements and approaches for this
502 issue will be discussed in section 5.3.

503 **5 Discussion**

504 **5.1 Results obtained versus available literature**

505 To the best of the author's knowledge, only few papers have evaluated the
506 environmental performance of MMC-based PHA production (Bengtsson et al., 2017;
507 Fernández-Dacosta et al., 2015; Gurieff and Lant, 2007; Morgan-Sagastume et al., 2016; Vega
508 et al., 2019), showing the scarcity of original data for the environmental validation of bio-based
509 products and biorefineries. Moreover, conflicting conclusions have been reported (Hottle et al.,
510 2013; Yates and Barlow, 2013), showing better environmental performances for GWP when
511 PHA is compared to PE (Gurieff and Lant, 2007), but generally worse when compared to PET
512 (Fernández-Dacosta et al., 2015).

513 Even when the impact assessment method and the categories selected are different in
514 each reference, some comparisons can be done between the results reported here and values
515 available in the literature. For example, Fernández-Dacosta et al. (2015) estimated a production
516 of 2.06 kg CO₂-eq/kg biopolymer, while 3.51 kg CO₂-eq/kg biopolymer was found for the
517 present study, being in the current literature range for MMC-based PHA. Although no absolute
518 values were reported, Morgan-Sagastume et al. (2016) found impact reductions for GWP, AP,
519 EP and POCP considering a volumetric unit of feedstock as FU. Their reduction values are
520 higher than the ones found in the present study, although in their case DSP was out of the
521 system boundaries.

522 Results suggest that the environmental and economic performance of PHA production
523 can be highly enhanced if it is integrated in existing plants (WWTP, biodiesel plants, hydrogen
524 production factories) adapting to seasonal and operational variations (Rodriguez-Perez et al.,
525 2018), or combining the production of several by-products, as biogas or compost (Morgan-
526 Sagastume et al., 2016; Vega et al., 2019). The present research work has assessed the potential
527 environmental benefits of PHA production from boiling mussel wastewater combining real data
528 from 2-year lab-scale operation and literature, responding to the urgent need of performing new
529 studies that can help to understand the implications of the integration of PHA production
530 processes in WWTP.

531 **5.2 Benefits of process integration strategies**

532 Energy consumption and DSP were identified in the past as bottlenecks for
533 environmental and economic validation of PHA production (Fernández-Dacosta et al., 2015;
534 Gurieff and Lant, 2007; López-Abelairas et al., 2015). Moreover, Fernández-Dacosta et al.
535 (2015) pointed out the non-negligible impacts related to heating (through steam) in the
536 fermenter unit to maintain adequate temperature for biological reactions, and identified DSP
537 as the main contributor to GWP category and energy consumption (60 % of GWP impacts and
538 72 % of non-renewable energy use).

539 In this respect, process integration was applied in this study through the use of MCW
540 excess energy in the DSP and for reactors heating, and through anaerobic digestion of the waste
541 sludge. Therefore, no heat was supplied to maintain process temperature neither in the
542 bioreactors nor in the DSP, saving approximately 500 kWh/day and 100 kWh/day, respectively.

543 Regarding DSP, energy consumption includes electricity and cooling energy (as
544 heating energy is avoided, Table 4). It accounts for 54 % of the total energy consumed in the
545 plant, while process integration saved about 15 % of the DSP needs, showing that an integral

546 approach could improve process feasibility (environmentally, but also economically). There
547 are only a few pilot-scale plants operating worldwide for PHA production from waste stocks
548 (Mannina et al., 2020), and studies up-scaling PHA production with waste feedstocks are still
549 scarce. Therefore, actual integration proposals are not yet specific and well defined, so potential
550 environmental benefits arising from process integration and energy optimization are being
551 disregarded from the assessment. This result shows a whole new path for the validation and for
552 the technical, economic and environmental optimization of bio-based products, although case-
553 by-case studies might be needed.

554 Concerning anaerobic digestion, although heat provided by the exhaust gases is enough
555 to maintain the digester temperature, the effect of anaerobic digestion in the overall process
556 performance is low, as most of the carbon present in MCW is employed for PHA production.
557 However, the implementation of anaerobic digestion avoids the release of harming emissions
558 linked to composting and generates electricity, enhancing the overall environmental
559 performance.

560 Moving to another topic, the results obtained also confirm the environmental benefits
561 of the combined production of PHA and biogas as reported by other authors, such as Vega et
562 al. (2019), who assessed the environmental performance of centralized biorefineries to produce
563 PHA and biogas using a mixture of cow manure and grape marc. This is linked to the idea of
564 second generation biorefineries, in which several resource recovery methods are combined and
565 different feedstocks can be treated, that is coming along as the future of bio-based products
566 (Dietrich et al., 2017). Although some potential improvement strategies were not included in
567 the present study due to uncertainties, they are mentioned here. First, the use of waste non-
568 PHA biomass coming from the DSP was excluded from the environmental evaluation, although
569 it contains carbon that could be used to improve biogas production. Second, the anaerobic

570 digester could be eventually transformed into a secondary VFA provider, improving system
571 productivity, and enhancing the plant capacity. Finally, the co-digestion of sludge and other
572 wastes coming from local industries could stimulate biogas production and increase the
573 economic and environmental benefits of the anaerobic digestion unit.

574 Finally, a centralized strategy was more beneficial than the current non-centralized
575 approach, although the transport stage had relevant impacts that need to be considered before
576 the centralized strategy is implemented (Figure 4b). Otherwise, the environmental benefit from
577 the biorefinery process could be offset by the impacts of transportation (Vega et al., 2019).

578 **5.3 Sensitivity analysis**

579 Figure 5 reported a better environmental performance for the circular economy
580 scenario, as its relative impacts are lower. In order to assess the robustness of those results, two
581 decisions are evaluated here: the alternative defined for sludge management and the final
582 PHA:PET equivalence (including extraction efficiency and replacement ratio).

583 Regarding the former, two new situations were modelled: anaerobic digestion without
584 energy recovery and composting. The circular economy scenario is still a favourable
585 alternative, even when no energy is recovered in the digester, compared to the current scenario
586 (Figure 6) for eight of the ten categories, being only DAR the impact category that changes
587 balance when no electricity is recovered (i.e. circular worse than linear based scenario), as the
588 digester energy needs (basically stirring) are no longer covered by the biogas production. Direct
589 emissions from the composting process and the removal of the benefits associated to energy
590 recovery identified this alternative as the worse one, being the circular based scenario no longer
591 the better option for DAR.

592 **FIGURE 6 AROUND HERE**

593 Concerning the latter, a replacement ratio (RR) PHA:PET of 1:1 was considered as no
594 better approximation was available. That ratio is dependent of the yield strength and the density
595 of the materials, and a recent study suggested that its value is of 0.93:1, i.e. 1 kg of PHA would
596 replace 0.93 kg of conventional PET in the plastic market (Vega et al., 2019). Besides, ideal
597 DSP efficiency was considered, that is to say, all the PHA entering the DSP process is
598 effectively extracted during the process. However, this efficiency is hard to estimate and is
599 dependent of several factors, such as the specific MMC used or the PHA content of the resultant
600 stream (Mannina et al., 2019). Averaging the results reported by (Fernández-Dacosta et al.,
601 2015) for PHA recovery yields using diverse DSP strategies, a value of 77.17 % is obtained.
602 Combining this value with the RR of 0.93, a replacement yield PHA:PET of 0.72:1 (i.e. 0.72
603 kg of PET production is avoided by each kg of PHA extracted from the Circular Economy
604 based Scenario) was applied and results are displayed in Figure 7.

605 FIGURE 7 AROUND HERE

606 The circular economy approach is still preferable to the non-centralized linear economy
607 current scenario, as average improvements of 25 % were found for all categories except DAR
608 and ODP. Not surprisingly, the worsening in fossil depletion category is linked to the lower
609 amount of avoided product (PET), being this lower the environmental benefits of the circular
610 economy approach are no longer present.

611 On the other hand, DSP is responsible for about 50 % of the impacts in the categories
612 that do not show any improvement compared to the circular economy scenario (DAR and
613 ODP). The significance of the DSP is not new (Gurieff and Lant, 2007; López-Abelairas et al.,
614 2015). Due to this fact, new research works are stepping forward towards new eco-friendly and
615 cost-effective extraction techniques, like the ones based on switchable anionic surfactants
616 (Mannina et al., 2019). The implementation of these new techniques could improve even more

617 the overall environmental response of the process and decrease the negative effects reported
618 for ODP category. Moreover, the DSP was included in the present study as new results covering
619 the whole PHA production process are demanded by the scientific community. However, the
620 answer to solve the DSP question may be linked to the creation of regional networks in which
621 WWTPs are high PHA-content biomass suppliers where the biopolymer is extracted in
622 centralized facilities (Morgan-Sagastume et al., 2016).

623 **5.4 Future outlook**

624 PHA production from MCW is still under development and optimization and, at
625 present, the overall process conversion is relatively low (0.2 g COD_{PHA}/g COD fed). Increasing
626 this process yield would increase environmental and economic benefits, and strategies such as
627 the combination of several substrates for PHA production (wastewater from other industries,
628 VFA coming from sludge management...) are potential ways to improve this efficiency
629 (Rodriguez-Perez et al., 2018).

630 The present research work focuses on one single type of wastewater, the MCW.
631 However, as stated in section 1, Galicia is responsible for about 80 % of the Spanish fish-
632 canning production. Once the production of MMC-based PHA under high salinity is validated
633 from a technical and environmental point of view, the possibilities are huge. One single fish-
634 canning facility can produce about 3,300 m³ of wastewater per day (Dirección Xeral de
635 Calidade e Avaliación Ambiental, 2008a), so assuming 6 % of high strength effluent each
636 facility could produce about 50 m³/day of a PHA-rich stream (containing 380 kg PHA) on-site.
637 Supposing 300 working days per year, and knowing that 7 of the top ten fish-canning
638 companies (in production and incomes) are located in Galicia (Eleconomista.es, 2018), the
639 annual regional potential is of 911 t PHA/year, which is near the minimum value reported by
640 Bengtsson et al. (2017) for economic feasibility. Four of these fish-canning plants are separated

641 less than 25 km, although the longest distance among facilities is of 100 km. Therefore, DSP
642 can be centralised for an optimized environmental and economic performance of bio-based
643 products, opening an unexplored scenario where technical, economic and environmental issues
644 need to be studied.

645 Finally, one challenge that is being faced by plastics and bioplastics industry is related
646 to end of life options (Geyer et al., 2017). Due to the lack of information, this study has
647 excluded them. Recent research works point out that mechanical recycling is preferable to
648 composting, incineration or landfilling for bio-based materials (Changwichan et al., 2018).
649 However, the effects of plastic litter in the water bodies, especially in the ocean, are still
650 unknown, and the actual effects of plastic pollution worldwide are uncertain. Initiatives such
651 as Plastic Leak Project⁹ or MarILCA¹⁰ will allow for better metrics to account for plastic
652 leakage and to integrate potential environmental impacts of marine litter, especially plastic, in
653 LCA results.

654 **6 Conclusions**

655 The renewable origin of bio-based plastics does not convert them automatically in an
656 environmentally sustainable products and, even when is clear that they are promising materials,
657 the environmental assessments comparing conventional plastics and bioplastics do not always
658 show explicit benefits.

659 This study presents a detailed analysis of the environmental performance of PHA
660 production from industrial wastewater, an area in which the LCA studies are still scarce. The
661 current linear economy approach for mussel cooking wastewater management (generation –
662 treatment – discharge) was compared with a circular economy approach, where PHA is

⁹ <https://quantis-intl.com/strategy/collaborative-initiatives/plastic-leak-project/>

¹⁰ <http://marilca.org/>

663 produced and wastewater is safely treated and discharged. A better environmental performance
664 was reported for nine out of the ten impact categories under evaluation, which reflects the
665 potential benefits of this novel approach. Process optimization through innovative systems (like
666 anammox reactors for nitrogen removal) come along as preferred choices to improve overall
667 performance (effluent quality and energy optimization).

668 The potential of bioplastics production processes is huge, although case-by-case studies
669 are needed, evaluating the local industries and waste streams availability, as well as PHA and
670 biogas yield for every feedstock. This study showed that the feasibility of producing added-
671 value bioproducts under a circular economy approach is linked to the integral vision of the
672 process, where all streams are valorised, and energy use is optimized. Finally, the potential of
673 Galician region for bioplastics production was estimated near 1 kt PHA/year, near the threshold
674 value for economic feasibility. Accordingly, centralized extraction facilities employing novel
675 extraction protocols could be the key for the environmental validation and the economic
676 viability of these products, stepping towards high-scale PHA production from mixed microbial
677 cultures.

678

679 **7 Acknowledgments**

680 This research was supported by the Spanish Government (AEI) through the
681 TREASURE project [CTQ2017-83225-C2-1-R]. USABLE Packaging project (H2020-BBI-
682 JTI-2018, EU ID: 836884) is also acknowledged. The authors belong to CRETUS Strategic
683 Partnership (ED4331e 2018/01) and the Galician Competitive Research Group (GRC ED431C
684 2017/29); both programs are co-funded by the FEDER (EU). Icons made by Smashicons,
685 Freepik, and DinosoftLabs from www.flaticon.com. The authors also want to acknowledge the
686 support provided by Ángeles Val del Río during the two years of operation of the reactors.

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