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1 Strategies for the valorisation of a protein-rich saline waste stream into 2 polyhydroxyalkanoates (PHA)

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6 Abstract

7 Saline Mussels Cooking Wastewater (MCW) was valorised to produce PHA
8 with Mixed Microbial Cultures (MMC). Due to the high protein content (1.8 – 5.7 g
9 COD_{PROT}/L), accumulating PHA capacity was initially below 10 %, so several
10 strategies were tested to improve it. In the acidification unit Na(HCO₃) was added,
11 which increased protein conversion to volatile fatty acids (VFA) from XX to XX %,
12 while the accumulation PHA capacity increased from 6.9 to 14.7 %. In the enrichment
13 unit the incorporation of a settling stage, after the feast phase, provoked a shift in the
14 protein's oxidation from the feast to the famine phase, which is desirable because the
15 nitrogen released in the famine is used by the MMC for growth, increasing the biomass
16 concentration and the load treated (XX). The last strategy was to feed the enrichment
17 unit with decreasing values of the proteins/VFA ratio, which allowed increasing the
18 PHA accumulation from 8.8 to 41.5 %.

19 **Keywords: Bioplastics; High salinity wastewater; Industrial Wastewater; Mixed**
20 **Microbial Cultures; Protein-rich waste streams.**

21 1. Introduction

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22 PHA are renewable, biodegradable and bio-based polymers produced by bacteria
23 which are expected to gradually replace conventional petrochemical plastics
24 (Kourmentza et al., 2017). In the last decade, the use of mixed microbial cultures
25 (MMC) and waste streams for PHA production has been explored to reduce overall
26 costs and environmental impacts (Roibás-Rozas et al., 2020; Yadav et al., 2020).
27 However, the use of waste streams for PHA production is challenging due to the
28 complexity of the substrate, containing substances that can be inhibitory for the
29 microbial activity (Korkakaki et al., 2016a; Palmeiro-Sánchez et al., 2019). The Spanish
30 north-western region of Galicia is responsible for the 90 % of the production of mussels
31 in the country, which is also the main mollusc producer of Europe (FAO, 2020). This
32 activity generates more than 100 M€ of incomes and more than 10,000 jobs in the
33 region (Rey-Méndez et al., 2016), and it is highly dependent on the water quality in the
34 estuaries where seafood is harvested. Because of this, a proper treatment of the effluents
35 generated in the fish-canning and fish-processing industries, normally located at shore
36 areas, is essential for the environmental and economic preservation of the region.
37 Nevertheless, the treatment of these effluents is challenging due to the presence of
38 potentially inhibitory compounds, such as sodium chloride or ammonia. More precisely,
39 the mussels cooking wastewater (MCW) contains high sodium chloride concentrations
40 (between 17.9-19.0 g NaCl/L), as well as sulphate and nitrogen (organic and in the form
41 of ammonia) in ranges that can be inhibitory for conventional processes, like the
42 anaerobic digestion (Palmeiro-Sánchez et al., 2013). In fact, several attempts were made
43 to valorise MCW in Galicia through biogas production. They were unsuccessful
44 possibly due to the complexity of the waste stream (Barros et al., 2009; Omil et al.,
45 1995), so the great concern regarding MCW treatment is reflected in local legislation

46 (Consellería de Medio Rural e Mar, 2015). Because of this, and its large biodegradable
47 organic matter concentration, the valorisation of MCW by PHA production was defined
48 as a possible alternative to treat these effluents. The Chemical Oxygen Demand (COD)
49 of MCW, ranging between 9.8-26.5 g COD/L, is about 95 % soluble and mainly
50 composed by proteins and carbohydrates. Carbohydrates are rapidly consumed in
51 fermentation processes, but proteins are consumed slowly. Furthermore, their presence
52 can provoke problems in the posterior aerobic PHA production units, so several
53 strategies, as uncoupling the carbon and nitrogen feeding or introducing a settling stage
54 in the process have been proposed (Argiz et al., 2020; Oliveira et al., 2017).

55 The aim of this research work is to evaluate how the presence of proteins affects
56 the MMC-based PHA production process and to assess the feasibility of using protein-
57 rich and saline wastewater as substrate. To do so, several long-term strategies were
58 tested in a three-stage system for PHA production, using a MMC fed with MCW: i)
59 alkalinity increase in the acidification unit; ii) settling stage in the PHA enrichment
60 reactor; iii) and decreasing proteins/VFA ratio fed to acclimate the MMC in the
61 enrichment unit. Then, these strategies were assessed and compared to choose the
62 optimal operational conditions.

63 **2. Material and methods**

64 **2.1 Experimental set-up**

65 A three-step system was utilized to produce PHA (see Supplementary Material
66 (SM)) as described in the following sections: a continuous stirred tank reactor (CSTR)
67 for acidification of the MCW (2.1.1); a sequencing batch reactor (SBR) for enrichment
68 of the MMC (2.1.2); and a fed batch reactor (FBR) for the accumulation of PHA (2.1.3).

69 The experimental stages tested in the continuous operation are summarized in Figure 1
70 and named as: A1-A6 for the acidification CSTR, E1-E5 for the enrichment SBR.

71 FIGURE 1 AROUND HERE

72 **2.1.1 Continuously Stirred Tank Reactor (CSTR) for acidification**

73 A CSTR was fed with MCW coming from a facility in Pontevedra, NW of
74 Spain. Although the main compounds of the MCW did not change throughout the
75 operational time, their concentrations fluctuated highly (see SM), so the Organic
76 Loading Rate (OLR) for CSTR stages ranged between 1.01 and 1.76 g COD/(L·d). It
77 had a volume of 5 L and it was operated as described in Fra-Vázquez et al. (2020). This
78 study started in the operational day 400, where Volatile Fatty Acids (VFA) were
79 produced steadily at a pH of 4.6 ± 0.6 with about 43 % of the effluent COD in the form
80 of VFA. The Solid Retention Time (SRT) was fixed equal to the Hydraulic Retention
81 Time (HRT), with a value of 6.25 days. The operational conditions by (Fra-Vázquez et
82 al., 2020) were first maintained (stage A1), but then, different amounts of sodium
83 bicarbonate were added (20 - 2700 mg NaHCO_3 /L of MCW in stages A2 to A6, see
84 Table 1) to increase the pH and improve protein solubility in the CSTR. The effluent
85 produced in the CSTR was stored at 4 °C until it was used in the following units.
86 Therefore, operational stages for the CSTR and SBR (explained in section 2.1.2) were
87 not synchronized, and their inter-relationship is also indicated in Table 1.

88 TABLE 1 AROUND HERE

89 **2.1.2 Enrichment Sequencing Batch Reactor (SBR)**

90 The inoculum of the SBR was enriched in PHA accumulating biomass
91 (accumulation capacity of XX), as it came from a similar bench-scale reactor that was

92 fed with the same MCW for a year, but this feeding was diluted with tap water to
93 decrease the salt concentration approximately to 5 g NaCl/L (Pedrouso et al. (2020)).
94 For the present work, salinity was gradually increased until to achieve the salinity of the
95 MCW (17-18 g NaCl/L) in 100 days by replacing the tap water by the effluent of the
96 same SBR as dilution agent, which means that the SBR effluent was recirculated to the
97 influent. Then, two different operational strategies (Cycles 1 and 2) were evaluated (see
98 SM): conventional and modified Aerobic Dynamic Feeding (ADF and M-ADF,
99 respectively). When the conventional ADF strategy (Cycle 1) was applied, air was
100 continuously supplied while, with the M-ADF one (Cycle 2), a settling and discharge
101 intermediate phases were included. In the case of Cycle 1, the exchanged volume was
102 50 % so the SRT and HRT of operation were equal to 1 day. For Cycle 2, no oxygen
103 was supplied during the settling and supernatant discharge phases, and aeration was
104 provided throughout the rest of the cycle phases. After settling, 25 % of the total reactor
105 volume (V_R) was withdrawn (supernatant discharge), so during the rest of Cycle 2, the
106 reactor operated with 75 % of the initial volume. As the initial feeding corresponded to
107 50 % of V_R and the final discharge was of 25 % of V_R , the SRT and HRT were of 2 and
108 1 days, respectively. The feeding of the SBR consisted of centrifuged CSTR effluent,
109 where the dilution agent was the settled (without solids) effluent of the same SBR. The
110 recirculation ratio (RR, i.e., volume of effluent from the CSTR / volume of effluent
111 from the SBR used as feeding) was established according to the composition of the
112 effluent produced in the CSTR and the organic load required to feed the SBR (Table 1).
113 The operation of the SBR was divided in six stages (from E1 to E6) depending on the
114 percentage of COD present as proteins (R_{PROT}) at the beginning of the cycles and on the
115 cycle type (ADF or M-ADF) (Figure 1). Allylthiourea was added to the feeding of the

116 SBR at 10 mg/L to avoid nitrification, antifoaming (0.5 mL/L of feeding) to prevent
117 spume problems and NaOH or HCl to maintain the pH value in the feeding
118 approximately neutral in stages from E3 to E6, but pH inside the reactor was not
119 controlled.

120 For all the stages, the reactor operated at 30 °C by using a thermostatic bath
121 (Techne Inc., USA), and air was supplied (6 L/min) through a ceramic air diffuser
122 located at the bottom of the reactor. As the CSTR effluent was not enough to achieve
123 the desired loads from stages E4 to E6, the SBR operation volume was reduced from 2
124 L (used from stages E1 to E3) to 1 L, maintaining all the operational conditions.

125 **2.1.3 Accumulation Fed-Batch Reactor (FBR)**

126 An FBR was employed to evaluate the maximal PHA accumulation capacity of
127 the enriched MMC. As inoculum it was used the biomass from the SBR and as feeding
128 the centrifuged effluent of the CSTR (containing VFA and the proteins) which was
129 added in pulses. Analysis of the liquid phase (data no shown) showed that VFA were
130 consumed first and proteins after, being possible to use the DO concentration value as
131 indicator. For this reason, each pulse of feeding in the FBR was supplied when the DO
132 concentration increased to intermediate values (approximately 4.0 - 4.5 mg O₂/L),
133 which marked that VFA was depleted and protein oxidation started.

134 To make assays comparable, the amount of VFA supplied in every pulse was set
135 as $15 \text{ Cmmol}_{\text{VFA}}/(\text{L}_{\text{reactor}} \cdot \text{pulse})$. Except on day 388, when pulses of 70
136 $\text{Cmmol}_{\text{VFA}}/(\text{L}_{\text{reactor}} \cdot \text{pulse})$ were used (increasing the volume of CSTR effluent in each
137 pulse). Therefore, in the accumulation assays the volume of the FBR varied from 0.5 to
138 1.0 L, and the volume of the pulses changed according with the CSTR effluent

139 acidification degree, so the working volume of the FBR varied in the different
140 experiments. Pulses were added until the accumulation assay achieved a maximum time
141 of 12 hours, which equal the enrichment cycle length.

142 The reactor temperature was maintained at 30 °C by using a thermostatic bath
143 (Techne Inc., USA), and air was supplied (6 L/min) through a ceramic air diffuser
144 located at the bottom of the reactor.

145 **2.2 Analytical methods**

146 Conductivity and pH were measured with glass electrodes (Hach-Lange 50-60
147 and Crisson GLP22 respectively), while Dissolved Oxygen (DO) concentration and
148 temperature were determined in the SBR and FBR with a probe (model HQ40d, Hach-
149 Lange, USA). Alkalinity, Total Suspended Solids (TSS), Volatile Suspended Solids
150 (VSS) and total COD (COD_T) concentrations were analysed in bulk samples, and the
151 dissolved matter was characterised after filtering with a cellulose-ester filter of 0.45 µm
152 pore size (Advantec, Japan), according to the Standard Methods (APHA-AWWA-WEF,
153 2017). Measuring included the following parameters: soluble COD (noted as COD in
154 the text) carbohydrates, proteins, Total Organic Carbon (TOC), Total Nitrogen (TN),
155 VFA, ammonium and other ions (Na⁺, Cl⁻, SO₄²⁻). COD was generally quantified
156 according to APHA-AWWA-WEF (2017), and based on the methodology described by
157 Soto et al. (1989) when samples had concentrations below 5 g COD/L. Carbohydrates
158 were measured as indicated in Dubois et al. (1956) and expressed as COD considering
159 that 1 g of glucose (used as standard) corresponds to 1.07 g of COD. Proteins were
160 analysed by the Lowry method (Lowry and Randall, 1951) and expressed as COD
161 considering that bovine serum albumin (used as standard) contains 1.32 g of COD and

162 0.15 g of N per gram of protein. TOC and TN concentrations were measured by
163 catalytic combustion in the TOC-L CNS analyser with the TNM-1 module (Shimadzu,
164 Japan). VFA concentrations were determined in a gas chromatograph (Hewlett Packard
165 5890A, USA) equipped with a flame ionization detector (FID) and an automatic injector
166 (Hewlett Packard 7673A, USA) and with ChemStation Rev. A. 10. 02 (1757) Agilent
167 Technologies software. Ammonium was quantified by the Bower/Holm Hansen method
168 (Bower and Holm-Hansen, 1980) and ions (Na^+ , Cl^- , SO_4^{2-}) by ion chromatography
169 (861 Advanced Compact IC, Metrohm, Switzerland).

170 PHA content was determined in biomass samples. To do so, unfiltered biomass
171 samples were centrifuged, and the supernatant removed. Then, the remaining pellet was
172 frozen and freeze-dried. The sample tube was weighed three times (empty, full of
173 sample and after freeze-drying) to calculate the total solids in the pellet (TS). The PHA
174 content (as g PHA/g VSS) was measured following the method described by Smolders
175 et al. (1994) for the quantification of the monomer propyl esters present in a lyophilized
176 sample. A commercial PHA standard (Sigma-Aldrich, USA) containing 88 % of
177 hydroxybutyrate (HB) and 12 % of hydroxyvalerate (HV) and benzoic acid as internal
178 standard were used. The propyl esters were analysed by means of gas chromatography
179 in a HP innovax column equipped with an FID (Agilent, USA). Biogas composition
180 (N_2 , CH_4 , CO_2 , H_2S) was analyzed in a gas chromatograph (Hewlett Packard, USA)
181 equipped with a packed column and a thermal conductivity detector (TCD) using
182 helium as carrier gas and the percentage of each compound was calculated by analyzing
183 1 mL of biogas injected with a syringe.

184 **2.3 Calculations**

185 **2.3.2 CSTR mass balances**

186 For the CSTR, the main parameters calculated were the acidification degree
 187 (Ac., Eq. (1)), protein and carbohydrates removal percentages (REM_{CARB} and
 188 REM_{PROT}), Eq. (2)) and VFA production ($COD_{VFAProd}$, Eq. (3)). In Eq. (1), COD_{VFA} is
 189 the concentration of VFA in the effluent (g COD/L). Subindex i represents whether the
 190 equation refers to carbohydrates or proteins. “INF” and “EFF” subindexes represent
 191 influent and effluent streams, respectively.

$$Ac. (\%) = \frac{COD_{VFA}}{COD} \cdot 100 \quad (1)$$

$$REM_i (\%) = \frac{COD_{i,INF} - COD_{i,EFF}}{COD_{i,INF}} \cdot 100 \quad (2)$$

$$COD_{VFAProd} = \frac{COD_{VFA,EFF} - COD_{VFA,INF}}{COD_{INF}} \quad (3)$$

192 2.3.3 SBR mass balances

193 For the SBR, the COD concentration at the beginning of an enrichment cycle
 194 (COD_0 , in g COD/L) was calculated according to eq. (4) because it has a 50 % of
 195 exchange volume ratio. Accordingly, the COD concentration of proteins or VFA at the
 196 beginning of the cycle ($COD_{i,0}$, g COD_i/L) was calculated as indicated in eq. (5).
 197 Analogously, this mass balance can be applied to calculate the concentration of the
 198 nitrogen forms in the cycle (substituting COD by TN or NH_4^+ -N, in mg N/L). Here,
 199 “INF” refers to influent (feeding stream) and “EFF” to the effluent of the previous
 200 cycle, which coincides in concentration with the remaining volume inside the reactor.
 201 The proportion of COD_{PROT} or COD_{VFA} over the total COD at the beginning of the SBR
 202 cycles (R_i , % (g COD_i/g COD)) is calculated as stated in eq. (6). The COD in the
 203 feeding of the SBR is mainly due to the presence of VFA and proteins, therefore R_{VFA} in
 204 the SBR cycles is (1- R_{PROT}).

$$COD_0 = \frac{COD_{INF} + COD_{EFF}}{2} \quad (4)$$

$$COD_{i,0} = \frac{COD_{i,INF} + COD_{i,EFF}}{2} \quad (5)$$

$$R_i = \frac{COD_{i,0}}{COD_0} \cdot 100 \quad (6)$$

205 A mass balance was performed to calculate protein consumption during the
 206 cycle. For conventional ADF, protein removal is only due to oxidation. However, for
 207 Cycle 2 (M-ADF), protein removal also occurs due to the withdrawal of the supernatant.
 208 Therefore, the protein removal rate due to oxidation ($REM_{PROT,OX}$, %) and to
 209 supernatant removal ($REM_{PROT,SUP}$, %) is calculated according to eq. (7) and eq. (8),
 210 respectively, where V_{SUP} is the volume of the supernatant withdrawal and V_R is the
 211 reactor volume at the beginning of the cycle after feeding addition (section 2.1.2).

$$REM_{PROT,OX} = \frac{COD_{PROT,0} \cdot V_R - COD_{PROT,SUP} \cdot V_{SUP} - COD_{PROT,EFF} \cdot (V_R - V_{SUP})}{COD_{PROT,0} \cdot V_R} \cdot 100 \quad (7)$$

$$REM_{PROT,SUP} = \frac{COD_{PROT,SUP} \cdot V_{SUP}}{COD_{PROT,0} \cdot V_R} \cdot 100 \quad (8)$$

212 For Cycle 1, V_{SUP} is zero, so $REM_{PROT,OX}$ is $(COD_{PROT,0} -$
 213 $COD_{PROT,EFF})/COD_{PROT,0}$. These mass balances can be applied for nitrogen forms by
 214 substituting COD_{PROT} by TN or NH_4^+-N . Finally, the protein variation during the cycle
 215 phases due to oxidation ($\Delta PROTOX$ in g PROT/L) is calculated as indicated in eq. (9):

$$\Delta PROTOX = \Delta PROTF + \Delta PROTFAM \quad (9)$$

216 Where $\Delta PROTF$ and $\Delta PROTFAM$ (both in g PROT/L) are the variation in the
 217 concentration of proteins during the feast and the famine phases, respectively, and they
 218 are calculated as indicated in eq. (10) and (11):

$$\Delta PROTF = PROT_0 - PROT_{MID} \quad (10)$$

$$\Delta PROTFAM = PROT_{EFF} - PROT_{MID} \quad (11)$$

219 Being $PROT_{MID}$ (g PROT/L) the protein concentration in the *middle* of the cycle
 220 (the point where feast finishes and famine begins). Accordingly, the percentage of
 221 COD_{PROT} oxidated during feast or famine ($REM_{PROT,F}$ or $REM_{PROT,FAM}$, in %) can be
 222 calculated by dividing $\Delta PROT_F$ or $\Delta PROT_{FAM}$ by $\Delta PROT_{OX}$ ².

223 2.3.4 PHA content and consumption/production rates

224 For the SBR and the FBR, PHA content in the cells (as percentage) is calculated
 225 according to equation (12). Specific consumption and production rates (q_{VFA} , q_{PROT} and
 226 q_{PHA} , in mg/(g X·h)) are estimated from the maximum slopes of the curves obtained
 227 from the corresponding experimental data, divided by the average active biomass (X,
 228 calculated as the subtraction of the mass of PHA to the mass of VSS measured). The
 229 active biomass composition was considered $CH_{1.8}O_{0.5}N_{0.2}$ for all the calculations. The
 230 biomass yield (Y_X) was estimated dividing the biomass production rate (g COD_X /h) by
 231 the VFA consumption rate (COD_{VFA} /h). Finally, the ratio r (g VFA/g proteins) is
 232 calculated by dividing q_{VFA}/q_{PROT} .

$$PHA \text{ (wt. \%)} = \frac{g \text{ TS} / L \cdot g \text{ PHA in sample} / g \text{ TS}}{g \text{ VSS} / L} \cdot 100 \quad (12)$$

233 3. Protein fermentation in the acidification reactor (CSTR)

234 The CSTR operated for 621 days in 6 operational stages according to the
 235 $Na(HCO_3)$ added in the feeding, which was increased from 0 to 2,700 mg/L to improve
 236 proteins solubility and promote their better degradation. Changes in the applied load (1 -
 237 1.76 g $COD/(L \cdot d)$), are due to the variability of the MCW (Table 1). From stages A1 to

² Note that $REM_{PROT,F}$ and $REM_{PROT,FAM}$ (%) can be expressed as g/g or g COD_{PROT} /g COD_{PROT} , to obtain the same result.

238 A5, pH in the CSTR was always below 5.0 due to VFA formation and low alkalinity,
239 because the added amount of $\text{Na}(\text{HCO}_3)$ was still not enough to clearly increase the pH
240 value. For stage A6, pH was around neutrality ($\text{pH} = 6.95 \pm 0.57$) due to the highest
241 added alkalinity dosage (2,700 mg $\text{Na}(\text{HCO}_3)/\text{L}$), so A6 corresponds to a neutral-pH
242 stage.

243 Carbohydrates were almost fully consumed (over 90 %) for every stage, but no
244 proteins (Figure 2). For acidic-pH stages (A1-A5) proteins removal ranged between
245 10.30 – 21.94 %, while for neutral-pH stage (A6) it increased to 42.45 ± 19.56 %. The
246 higher proteins removal promoted an increase in the $\text{COD}_{\text{VFAProd}}$ and acidification from
247 0.21 – 0.28 g $\text{COD}_{\text{VFA}}/\text{g COD}$ and XX % (in A1-A5) to 0.43 ± 0.12 g $\text{COD}_{\text{VFA}}/\text{g COD}$
248 and 71.59 ± 13.05 % (in A6), respectively. Therefore, the increase in $\text{COD}_{\text{VFAProd}}$ and
249 acidification percentages for the neutral-pH stage can be attributed to the increase in the
250 protein consumption associated to the modified pH-environmental conditions.

251 Successful acidification of the MCW was achieved and no methane was detected
252 during the whole operational time. For stages A1-A5 (acidic-pH), the inhibition of
253 methanogenic activity can be attributed to the low pH of operation (below 5) caused by
254 VFA accumulation (Fra-Vázquez et al., 2020), but this cannot be the reason for the
255 inhibition for the neutral-pH stage (stage A6). Although high concentrations of salt, and
256 in special sodium ion, can inhibit methanogenic activity, methane can appear in long-
257 term operations despite high salinity (Palmeiro-Sánchez et al., 2013). However, when
258 sulphate is present in the wastewater and the $\text{COD}/\text{SO}_4^{-2}$ ratio is below 10 g/g,
259 methanogens are inhibited due to their competition with sulphate reducing bacteria. In
260 this case, the complex matrix of MCW makes this waste stream ideal for VFA
261 production, as it has high concentrations of sodium due to salinity, and a $\text{COD}/\text{SO}_4^{-2}$

262 ratio below 10 g/g, which inhibits methanogens. Therefore, the compounds present in
263 the MCW caused the absence of methanogenic activity during all the CSTR operation.

264 The transformation of proteins into VFA in anaerobic mixed culture
265 fermentations has generated increasing interest in the last years (Bevilacqua et al., 2020;
266 Jin et al., 2016; Liu et al., 2015; Regueira et al., 2020a, 2020b; Yang et al., 2015), as
267 they are degraded slower than carbohydrates. Hydrolysates of proteins and
268 carbohydrates are peptides/amino acids and glucose, respectively. As the presence of
269 glucose represses protease formation, the uptake of glucose/carbohydrates happens first
270 (Yang et al., 2015). Moreover, pH is one of the most relevant factors regarding VFA
271 production from proteins (Regueira et al., 2020a). When pH is low and VFA are
272 formed, undissociated acids cross the membrane, releasing protons inside the cell and
273 inhibiting the generation of new acids. Furthermore, as the concentration of protons in
274 the solution increases, the interaction of hydrogen bonds becomes stronger. Thus, the
275 solubility of proteins decreases, as they aggregate and even coagulate at low pH values
276 (Liu et al., 2015). This can explain the results of the CSTR operation, where
277 carbohydrates are always consumed and proteins uptake only happens at the neutral-pH
278 (stage A6).

279 FIGURE 2 AROUND HERE

280 **4. Enrichment (SBR) and accumulation (FBR) reactors**

281 The SBR was operated during 540 days, and the experimental time was divided
282 in six stages (Figure 1), selected according to: a) CSTR operational conditions
283 (generating an acidic-pH or neutral-pH feeding), b) proportion of COD_{PROT} in SBR
284 cycles (if R_{PROT} is higher than 50 %, it is a high- COD_{PROT} stage; if R_{PROT} is below 50

285 %, it is a low-COD_{PROT} stage and, consequently, a high-COD_{VFA} stage), and c)
286 enrichment strategy (ADF or M-ADF). A recirculation was performed in four of the
287 stages (Table 1) with the aim of reaching stable salt concentrations avoiding the use of
288 tap water for dilution and load control. The maximum concentrations of 28.3 ± 0.7 g
289 NaCl/L in the SBR-FBR corresponded to the use of saline wastewater (19 g NaCl/L),
290 the addition of alkalinity as Na(HCO₃), and NaOH for feeding pH control, so the raise
291 was gradual (data not shown) to let the biomass adapt to the highly saline conditions.

292 **4.1 SBR operation using acidic-pH feeding**

293 Proteins were always present in the SBR feeding, although their proportion
294 regarding the COD fed (R_{PROT}) varied (Figure 3a). To unravel the effect of proteins on
295 the enrichment process, two operational strategies were tested by applying the two
296 previously defined cycle distributions (ADF and M-ADF) to two levels of protein (high
297 and low R_{PROT}).

298 **FIGURE 3 AND TABLE 2 AROUND HERE**

299 **4.1.1. High R_{PROT} and conventional ADF**

300 The enrichment of PHA-accumulating organisms was initiated applying an ADF
301 regime (stage E1). Along with the 100 % consumption of VFA (data not shown),
302 approximately 34.7 % of the proteins were removed in each cycle during the feast
303 period (Table 2, Figure 3b). Therefore, the MMC consumed proteins simultaneously to
304 VFA. The presence of non-VFA COD in the enrichment process (like proteins) can be
305 harmful for the selection, as carbon is used by non-storing populations to grow and
306 proliferate in the system (Argiz et al., 2020). This issue was explored by (Korkakaki et
307 al., 2016b) for a system with methanol and VFA, where they proposed the parameter r

308 ($q_{\text{VFA}}/q_{\text{MeOH}}$) as a control for the enrichment success. They found that r needs to be
309 equal to or higher than 4.7 g HAc/g MeOH (or 5 Cmol HAc/Cmol MeOH) for MMC
310 selection to be effective. Here, r ($q_{\text{VFA}}/q_{\text{PROT}}$) had values of 0.81-2.60 g VFA/g protein
311 (Table 2), indicating poor MMC selection, which in certain periods consumed proteins
312 even faster than VFA. Hence, maximal PHA-accumulation capacities of the MMC from
313 E1 in the FBR were always below 10 % (Table 2).

314 **4.1.2. High R_{PROT} and M-ADF**

315 Later, the cycle distribution of the SBR was modified to M-ADF (Stage E2), so
316 a settling phase was introduced to improve MMC selection. After withdrawal the
317 removed volume (which was 25 % of V_{R}) was not substituted with any other stream due
318 to the inexistence of a current with the same composition of the acidified wastewater but
319 without proteins, thus only 75 % of the initial volume remained inside the reactor during
320 the rest of the cycle. Except for the beginning of E1, where the applied load was still
321 being adapted, the SBR operated in E1 and E2 at similar COD_0 and $\text{COD}_{\text{VFA},0}$ (Table 1,
322 Figure 3a). For similar loads, r value generally increased from values below 3 g/g in E1,
323 to values over 3 g/g in E2 (Table 2), indicating the MMC selection amelioration.
324 Although the r value previously mentioned of 4.7 g HAc/g MeOH corresponded to a
325 simple substrate (methanol), more complex substrates (as protein) could yield in a lower
326 minimum r threshold.

327 Furthermore, a decrease in the protein oxidation by the MMC was observed with
328 the change in the cycle type. Protein removal was about 35 % in E1, while it was around
329 47 % in E2. However, for E2, 20 % of the removal happened due to supernatant
330 withdrawal, so oxidation by the MMC was only 27 %. Moreover, for E1, removal

331 happened basically during feast, while, for E2, proteins were consumed mostly during
332 famine phase. Even so, the accumulation capacity of the MMC did not significantly
333 increased in E2 (Table 2). It was observed that, when a high R_{VFA} (%) was applied to
334 the SBR prior to the accumulation experiments in FBR (day 244 of operation), the
335 MMC storing response improved. The accumulating capacity of the MMC in the FBR is
336 highly dependent on the R_{VFA} (%) applied to the SBR: an R_{VFA} increase stimulate the
337 storing response of MMCs (de Oliveira et al., 2019; Lorini et al., 2020). In fact, the
338 accumulation capacity of the MMC in the FBR seemed to be boosted only by the R_{VFA}
339 (g COD_{VFA} /g COD_0) of the SBR (Figure 4). Apparently, this behaviour is independent
340 of the selection strategy applied (AFD, M-ADF).

341 FIGURE 4 AROUND HERE

342 On the other hand, the research studies carried out in the last years aim to
343 incorporate the PHA production process in the wastewater treatment system to
344 transform treatment lines into valorisation trains. Therefore, the production of PHA
345 must be simultaneous to the removal of pollutants compounds. In this sense, the
346 enrichment of the MMC can be simultaneous to processes involved in the biological
347 nitrogen removal, like the partial nitrification (Fra-Vázquez et al., 2019), the
348 nitrification/denitrification (Basset et al., 2016; Frison et al., 2015) or the denitrification
349 (Santorio et al., 2019). Nevertheless, for carbonaceous compounds not useful for PHA
350 production (like proteins), the preferred strategy consists of removing them from the
351 system through a settling stage after the end of the feast phase which will also increase
352 the concentration of storing populations (Argiz et al., 2020; Korkakaki et al., 2016b;
353 Mulders et al., 2020). Moreover, when dealing with proteinaceous wastewater, it is also

354 common to remove them through other means prior to the enrichment process
355 (Colombo et al., 2019).

356 Here, in stage E2, the MMC partially lost its capacity of consuming proteins.
357 Hence, COD_{PROT} is present in the reactor outflows (supernatant and effluent streams,
358 Figure 3b), meaning that, from a full-scale approach, further treatment would be needed
359 before discharge. Uncoupling the carbon and nitrogen supply in the enrichment reactor
360 has been successfully applied with protein-rich streams (Oliveira et al., 2017), but the
361 supply of nitrogen is performed through the addition of chemicals, so the industrial
362 application of this strategy can be hindered due to economic and environmental issues.
363 Therefore, new strategies were tested to assess if PHA production and protein removal
364 can occur in the same SBR cycle.

365 To do so, an strategy with decreasing proteins/VFA ratio fed was tested in E3.
366 Here, the COD_0 was maintained in the same range as in E2, but the $COD_{VFA,0}$ was
367 varied as follows: at the beginning of E3 (days 265 to 280), the feeding of the SBR
368 consisted of raw MCW (non-acidified) and recirculated SBR effluent. Therefore,
369 $COD_{VFA,0}$ was negligible, while the protein content was maintained at the same levels as
370 in prior stages (Figure 3a). Then, raw MCW was gradually substituted by the fermented
371 MCW coming from the CSTR, decreasing the proteins/VFA ratio. For E3, PHA
372 accumulation increased in the SBR (below 10 % in E2, above 10 % in E3) along with
373 protein oxidation (from 27 % in E2 to about 32 % in E3). Moreover, proteins were still
374 consumed mainly in famine ($REM_{PROT,FAM}$ was 64.3 %, Table 2).

375 **4.1.3. Low R_{PROT} and M-ADF**

376 In stage E4 the CSTR effluent was directly fed to the SBR with no dilution, so
377 R_{VFA} was higher than 50 % for the first time throughout the experimental period. The
378 protein elimination in the SBR in this stage was about 72 %, with an 18 % due to the
379 supernatant removal. Removal by oxidation (54 %) occurred in a 36 % in the feast and
380 64 % in the famine phases, so the protein consumption distribution in E4 were like that
381 in E3 and E2 (mainly during famine). The PHA-storing capacities of the biomass in this
382 stage were also the highest, exceeding the 40 % in the FBR and being of approximately
383 20 % in the SBR, with an r value of of 3.7 g/g. Therefore, proteins were consumed
384 simultaneously to MMC enrichment in the SBR. The reached accumulation percentage
385 (41.5 % of PHA in the FBR) exceeded the threshold value established for economic
386 feasibility (Bengtsson et al., 2017), and it is similar to other results obtained in systems
387 working with high proteins and/or salinity concentration. Hao et al. (2017) reported 42.3
388 % of PHA accumulation when they used fermented sludge with high protein content,
389 and Wen et al. (2018) obtained 42.6 % of PHA when they employed fermented leachate
390 at 15 g NaCl/L and 1.3 g COD/(L·d) in the SBR.

391 Besides, the biomass concentration was maximized, averaging 4.2 ± 1.8 g
392 VSS/L in the SBR effluent, with the highest q_{PHA} and the lowest Y_X for all the stages
393 tested (Table 2). When proteins were assimilated in stage E4, the total nitrogen
394 consumption in SBR cycles (measured as the sum of organic and inorganic nitrogen
395 forms, see SM) is higher than the apparent ammonium nitrogen consumption during the
396 cycles. This indicates that the nitrogen released by the proteins is employed by the
397 MMC for growth. So, as more nitrogen is available, the concentration of biomass
398 increased to reach its highest value in E4 (Table 2), and higher organic loads are
399 tolerated.

400 To the best of our knowledge, few works have explored the effect of proteins in
401 enrichment reactors. Jia et al. (2013) fed an SBR for the enrichment of an MMC with
402 simulated excess sludge fermentation liquid, so a mixture of synthetic VFAs was
403 initially used. Then, bovine serum albumin was added to the SBR feeding to test its
404 effect on the enrichment process. Although the addition of proteins worsened the
405 enrichment performance, the results showed that its consumption during the cycle
406 facilitated the cell growth. Moreover, a clear deterioration of the accumulation dynamic
407 was found when R_{PROT} (g COD_{PROT} /g COD) was higher than 30 % in SBR feeding.
408 Here, with the applied loads in stage E4, the R_{VFA} was 61.36 ± 9.97 %, and the best
409 results were achieved in day 334, when R_{VFA} was as high as 69.9 % (so R_{PROT} was
410 about 30 %). In fact, when Hao et al. (2017) used the guidance provided by Jia et al.
411 (2013) to treat the excess sludge fermented liquid (containing proteins and
412 carbohydrates), they achieved good results despite the presence of non-VFA organic
413 matter.

414 Finally, Tu et al. (2020) harvested the biomass of a MMC in an enrichment
415 reactor just after the feast phase. Then, the famine period was carried out in batch assays
416 where different concentrations of non-VFA COD were added. In their study a
417 worsening in the enrichment performance was detected, as internal PHA at the end of
418 the cycle was higher than for cycles without addition of non-VFA COD. However, a lag
419 phase in the profile of PHA consumption of the stored carbon was detected in the MMC
420 while non-VFA COD was consumed. This suggested that the microorganisms capable
421 of storing PHA can also choose the substrate to be consumed (internal or external) when
422 both are available.

423 Therefore, although high concentrations of proteins are harmful for the
424 accumulation process (above 30 % of the COD), their presence can stimulate the system
425 dynamics, as proteins are non-VFA COD, but they are also nitrogen and carbon sources.
426 Moreover, protein consumption releases nitrogen, that will be used by the two present
427 populations (storing and non-storing) for growth in the famine phase. Consequently,
428 proteins can enhance the process performance if a dynamic balance is established in the
429 reactor medium and if proper acclimation and selection strategies are applied as
430 demonstrated here.

431 Consequently, the imposed enrichment strategy (ADF or M-ADF) is not directly
432 responsible of an increase in the MMC accumulating capacity. However, the imposition
433 of a proper selection dynamic and of a second selective pressure (the settling stage) is
434 necessary to increase the applied load that will rise the storing response. Moreover, the
435 presence of proteins can be beneficial for the system if R_{VFA} is about 70 %, as the
436 released nitrogen due to protein uptake can be used by biomass for growth. As more
437 biomass is available, the tolerated loads will be higher and PHA production can be
438 increased.

439 Finally, because of the optimized behaviour in the system, two different
440 accumulation approaches were tested as indicated in Section 2.1.3. The best results were
441 obtained when 15 Cmmol/(L·pulse) were applied (day 334) (Table 2).

442 **4.2 SBR operation using neutral-pH feeding**

443 **4.2.1 High R_{PROT} and M-ADF**

444 The proteins present in the SBR feeding in stage E5 were the ones not
445 transformed into VFA in the CSTR in A6 (operated at 6.25 days of residence time and

446 neutral pH), so proteins were less available for the MMC. Because of this, when the
447 applied loads of E4 were tested in E5 (COD_0 was 4 – 5 g COD/L, Figure 3a), the feast
448 phase lasted 6-8 hours (feast length lasted about 2.75 hours for steady operation, see
449 SM), and the biomass concentration in the reactor decreased to 2.7 ± 1.1 g VSS/L
450 (Table 2). Due to this instability, accumulation cycles could not be performed and, to
451 attain steady state conditions, the applied load was diminished down to reach a COD_0 of
452 2 – 3 g COD/L and R_{PROT} increased due to recirculation. When no proteins are
453 available, the selection of the MMC is supposed to be improved, as the concentration of
454 non-VFA forms of COD decreases. However, as less nitrogen is available, less growth
455 is promoted so the biomass concentration at the end of the cycle decreases, and organic
456 load needs to be reduced to maintain the accumulation dynamic.

457 In stage E5, the value of r increased to its highest level basically because
458 proteins were slightly consumed. However, PHA storing decreased to 14.03 % in the
459 SBR since the applied load could not be raised due to excessively length of the feast
460 periods (6-8 hours) and the occurrence of the biomass loss. Moreover, q_{PHA} for the
461 enrichment cycles in the stage E5 presented the lowest values of any tested stage of 8.9
462 mg PHA/(g X·h) and protein oxidation decreased to 28.2 %. Nevertheless, it still
463 happened during the famine phase (like in the other stages with M-ADF).

464 **4.2.1 High R_{PROT} and ADF**

465 In stage E6, the settling phase was removed from the cycle and the ADF strategy
466 was imposed as in the stage E1. Here, although protein removal due to oxidation
467 decreased to 23.5 %, the accumulation in the SBR and FBR worsened to values of

468 5.09 % and 14.66 %, respectively. Moreover, protein consumption occurred during the
469 feast phase for the two stages where conventional ADF was tested (E1 and E6, Table 2).

470 Generally, when proteins are consumed during the feast phase of the cycle, the
471 enrichment process is unsuccessful (Korkakaki et al., 2016b; Oliveira et al., 2017).
472 Although their presence is normally considered undesirable, protein consumption
473 during the famine stage can promote biomass growth without negatively affecting the
474 enrichment performance when its presence is lower than 30 % of the COD (Jia et al.,
475 2013). In the present study, although the enrichment strategy did not directly affect the
476 accumulating capacity for the same applied loads, it had clear and significant impact on
477 the protein consumption profile. For the stages with ADF strategy (only relying on the
478 FF regime), proteins were totally or mainly consumed during the feast phase of the
479 cycle, but, when the M-ADF strategy was imposed, they were consumed mostly during
480 the famine phase. Therefore, M-ADF improved the culture selection, while protein
481 consumption during famine was linked to an increase in the concentration of
482 accumulating microorganisms. Finally, as storing populations proliferated and biomass
483 concentration was higher, the tolerated loads and the PHA accumulation raised.

484 Summing up, the enrichment strategy did not directly affect the storing capacity
485 (it is only boosted by the load increase), but it does indirectly as a load raise is only
486 possible if a proper enrichment strategy (M-ADF) is applied. Therefore, proper
487 selection of the culture (where non-VFA forms are present) is only possible if two
488 selective pressures are imposed.

489 Again, the maximum COD_0 tolerated by the system was 2 – 3 g COD/L, so
490 R_{PROT} increased due to dilution. Moreover, a change in the enrichment strategy reversed

491 the SBR behaviour, which presented similar r values and biomass concentration than in
492 stage E1, while protein oxidation occurred again during famine (as in E1, Table 2).
493 Therefore, for the same operational strategy but lower protein availability, the system
494 performance was not improved in E5 although protein consumption was lower with
495 respect to stage E1.

496 **5. Conclusion**

497 Proteins conversion into VFA in the acidification unit was enhanced from XX
498 to XX % with the addition in the feeding of Na(HCO₃) to have neutral pH. In the
499 enrichment unit, proteins can be beneficial (at concentrations below 30 % of COD) if
500 the enrichment strategy includes a settling stage to promote their consumption in the
501 famine, because nitrogen is released and used for biomass growth. Therefore, as
502 biomass concentration increases, the load tolerated and the amount of PHA produced by
503 the system are higher. Finally, the decrease of the proteins/VFA ratio to acclimate the
504 MMC to proteins, allowed increasing the PHA accumulation from 8.8 to 41.5 %.

505

506 E-supplementary data of this work can be found in online version of the paper.

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513 **7. Author contributions**

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518 editing, Supervision, Project administration, Funding acquisition. **Almudena Hospido:**
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677 **TABLES AND FIGURES**

678

679 Table 1: Operational Stages throughout the operation of the acidification (CSTR) and
680 the enrichment units (SBR).

681 Table 2: Main results obtained by the monitoring of operational cycles in the
682 enrichment and accumulation reactors.

683 Figure 1: Operational stages in the three-stage PHA production system. Continuous
684 lines represent the operational stages and dashed lines represent the mass balances for
685 each stage. The boxes filled with diagonal grey lines for the enrichment stages represent
686 the periods where the volume of the reactor was reduced from 2 L to 1 L. fMCW is the
687 acidified effluent of the Continuously Stirred Tank Reactor (CSTR).

688 Figure 2: Protein Removal (REM_{PROT} , \square), carbohydrates removal (REM_{CARB} , \blacksquare), and
689 Acidification Degree (Ac, Δ), expressed as percentages, and VFA production
690 ($COD_{VFAProd}$ \circ , $g\ COD_{VFA}/g\ COD_{INF}$) in the CSTR.

691 Figure 3: a) COD concentration at the beginning of SBR cycles: COD_0 (\circ), $COD_{VFA,0}$
692 (\blacksquare) and $COD_{PROT,0}$ (\bullet), in $g\ COD/L$. b) Protein concentration in SBR: in the influent

693 $(\text{COD}_{\text{PROT,INF}} \blacklozenge)$, at the beginning of the cycle $(\text{COD}_{\text{PROT,0}} \bullet)$, in the supernatant
694 $(\text{COD}_{\text{PROT,SUP}} \blacktriangle)$, and in the effluent $(\text{COD}_{\text{PROT,EFF}} \square)$, expressed as g $\text{COD}_{\text{PROT}}/\text{L}$.
695 Figure 4: Relationship between R_{VFA} (%) in the SBR and the stored PHA (%) in the
696 FBR, for experiments without settling (Cycle 1, ADF) (\circ) and with settling phase
697 (Cycle 2, M-ADF) (\bullet).

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699 **Table 1**

Acidification Reactor (CSTR)					Enrichment Reactor (SBR)						
Stage	Na(HCO ₃) (mg/L of feeding)	Days	OLR (g COD/(L·d))	Stage in SBR ^(a)	Stage	Days	Cycle	COD _{VFA,0} (g COD _{VFA} /L)	R _{VFA} , % (g COD _{VFA} /g COD)	SRT (days)	RR ^(b)
A1	0	0-263	1.01 ± 0.21	E1-E2	E1	0-205	ADF	0.50 ± 0.26	34.98 ± 16.79	1	1:4
A2	20	264-332	1.27 ± 0.13	E2-E2a	E2	206-263	M-ADF	0.71 ± 0.11	32.02 ± 7.32	2	1:5
A3	80	333-395	1.44 ± 0.23	E3	E2a	264-335	M-ADF	0.72 ± 0.32	33.19 ± 14.22	2	1:6 to 1:1
A4	320	396-466	1.76 ± 0.21	E3	E3	336-425	M-ADF	2.69 ± 0.75	61.36 ± 9.97	2	1:1 or 1:0
A5	640	467-502	1.75 ± 0.21	E4	E4	425-498	M-ADF	1.75 ± 0.48	51.28 ± 8.84	2	1:1 to 1:3
A6	2700	503-621	1.48 ± 0.42	E4-E5	E5	499-536	ADF	0.94 ± 0.37	36.98 ± 4.73	1	1:4

700 ^(a) CSTR effluent was stored until used, so the operational time is not always coincident. This column shows the link between the effluents obtained in each acidification
701 CSTR operational stage (employed as SBR feeding) and the SBR operational stage.

702 ^(b) RR: Recirculation ratio to the SBR (CSTR effluent volume : SBR recirculated effluent volume).
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711 **Table 2**

Stage	E1 (ADF)		E2 (M-ADF)		E3 (M-ADF)		E4 (M-ADF)		E5 (M-ADF)		E6 (ADF)	
Protein removal in SBR: total, due to oxidation (REM_{PROT,OX}) and due to supernatant withdrawal (REMP_{PROT,SUP})												
Average Total Protein Removal ⁽¹⁾	34.7		47.4		46.3		71.8		52.9		23.5	
Oxidation (%)	34.7		27.0		31.9		53.6		28.2		23.5	
Withdrawal (%)	-		20.4		14.4		18.1		24.8		-	
Protein oxidation distribution over the enrichment cycles: during feast (REM_{PROT,OX,F}) and during famine (REM_{PROT,OX,FAM})												
Feast (%)	98.2		25.7		35.7		37.1		0.0		100.0	
Famine (%)	1.8		74.3		64.3		62.9		100.0		0.0	
Biomass concentration at the end of SBR cycles												
Biomass (g VSS/L)	1.3 ± 0.7		2.5 ± 0.5		1.6 ± 0.4		4.2 ± 1.8		2.7 ± 1.1		1.4 ± 0.2	
CYCLES												
SBR												
Day	11	88	123	187	228	244	255	302	318	349	473	513
PHA (%)	12.4	11.5	3.5	3.6	5.4	8.2	6.7	14.6	11.0	18.8	14.0	5.1
q _{PHA} (mg PHA/(g X·h))	18.5	24.7	20.5	49.8	27.5	49.9	37.3	-	-	21.68	8.9	14.0
r (q _{VFA} /q _{PROT}), g/g	1.5	2.6	0.81	1.3	6.0	6.0	3.2	-	-	3.7	36.2	1.5
FBR												
Day	97		139		236		250		257		508	
PHA (%)	6.9		7.8		7.3		17.8		8.8		14.7	
q _{PHA} (mg PHA/(g X·h))	13.2		10.0		13.9		6.3		17.2		24.5	
Y _X (g COD _X /g COD _{VFA})	14.2		49.2		49.5		33.3		31.2		9.2	
CONDITIONS OF SBR CYCLE PREVIOUS TO THE FBR-ACCUMULATION ASSAY												
COD ₀ g COD/L	2.0		2.5		2.5		2.0		2.1		2.6	
R _{VFA} (%)	19.1		31.9		29.6		46.6		29.9		37.8	

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⁽¹⁾ The average protein removal is calculated using the protein concentration measured twice weekly in the SBR streams during each operational stage. The protein oxidation taking place in the feast or famine phases is calculated using the data obtained in the cycles monitored monthly throughout the operational time. Standard deviations of the elimination percentages are not provided because the wastewater composition was highly variable, so the propagation of uncertainty due to this variability generated extremely high and non-representative dispersions.

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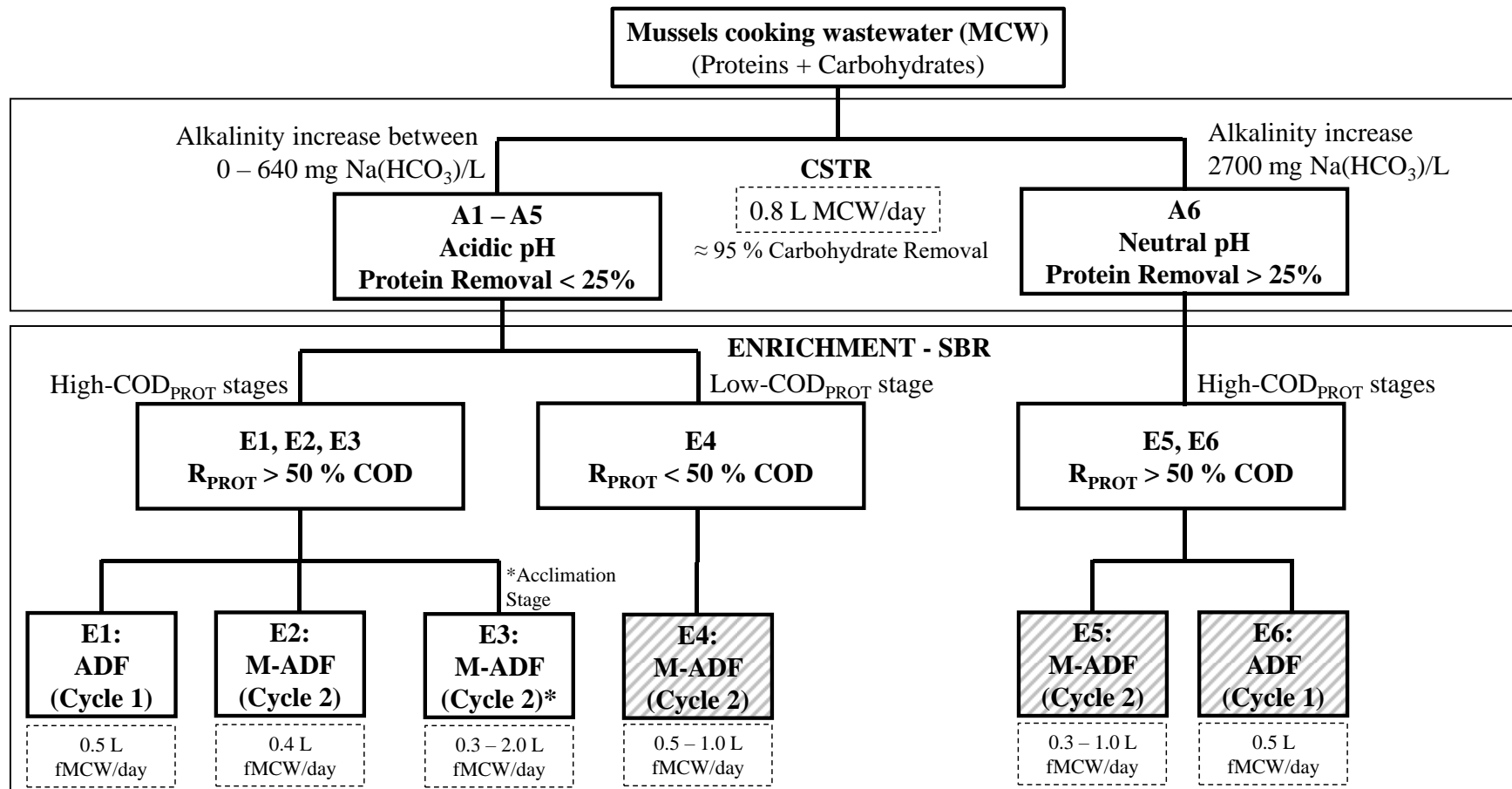


Figure 1

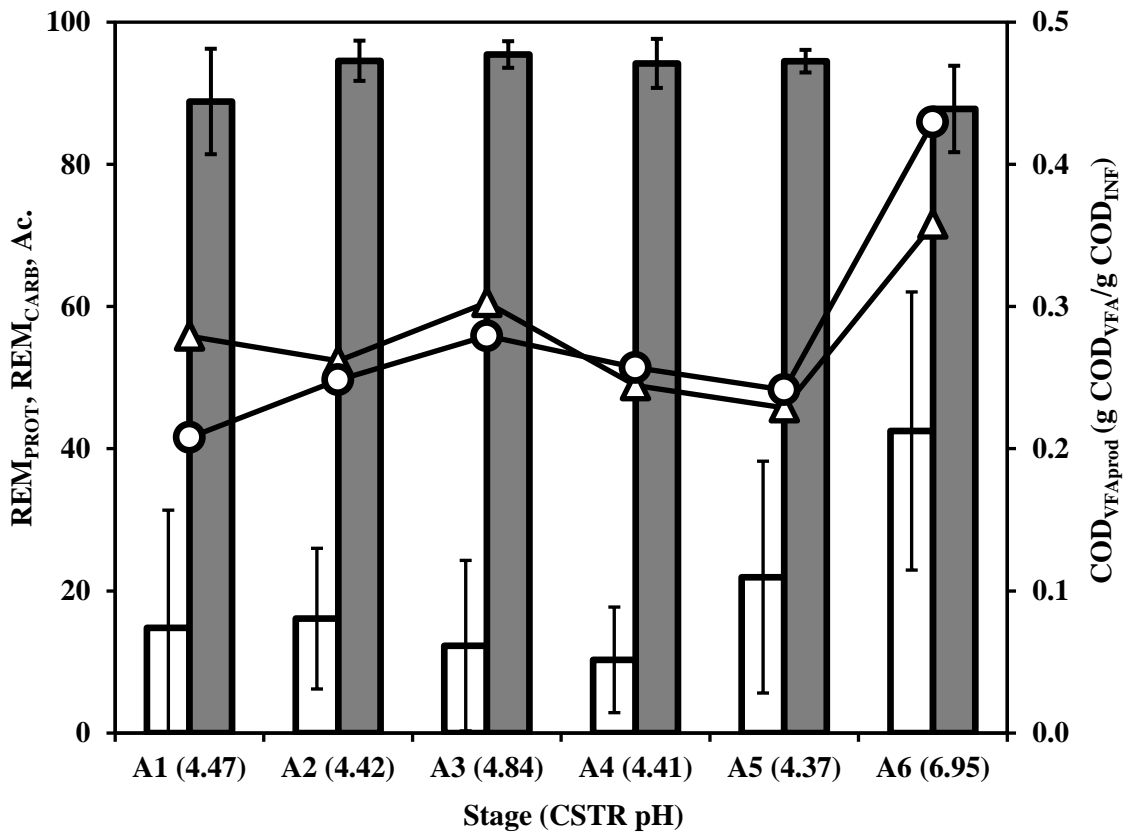
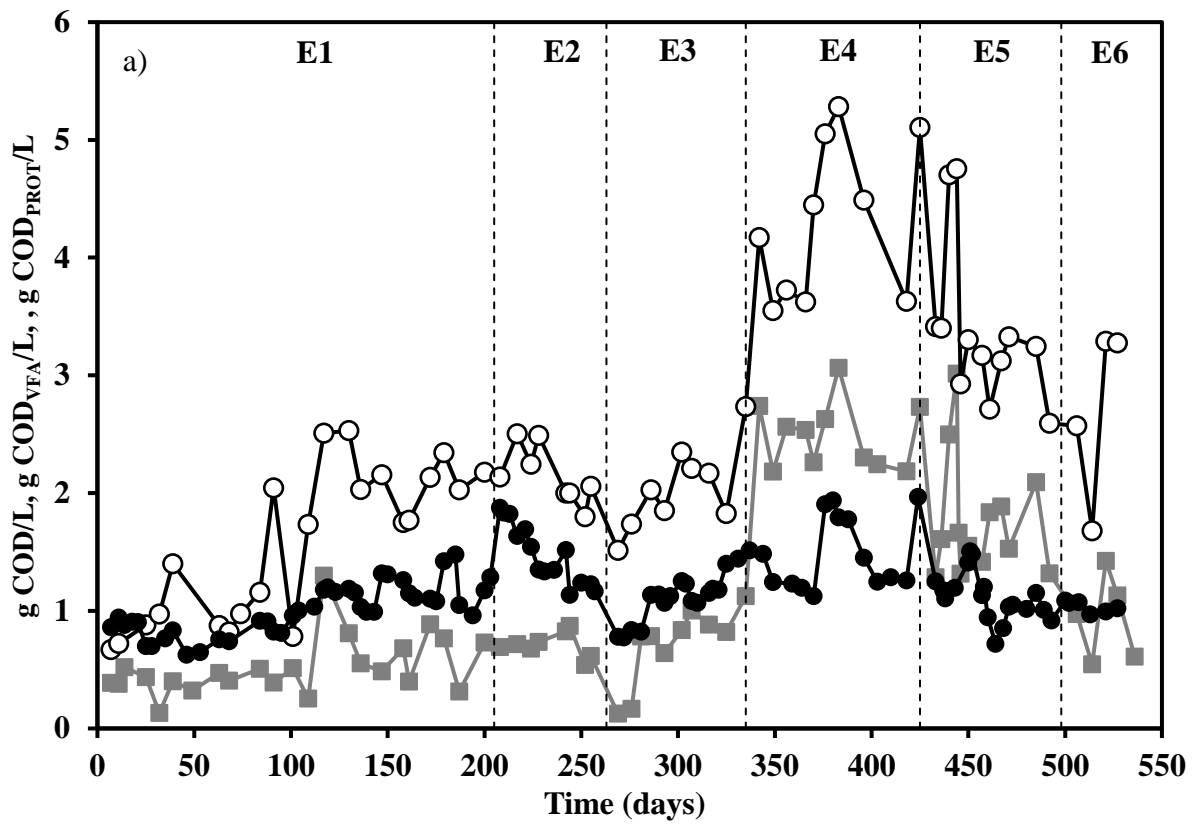
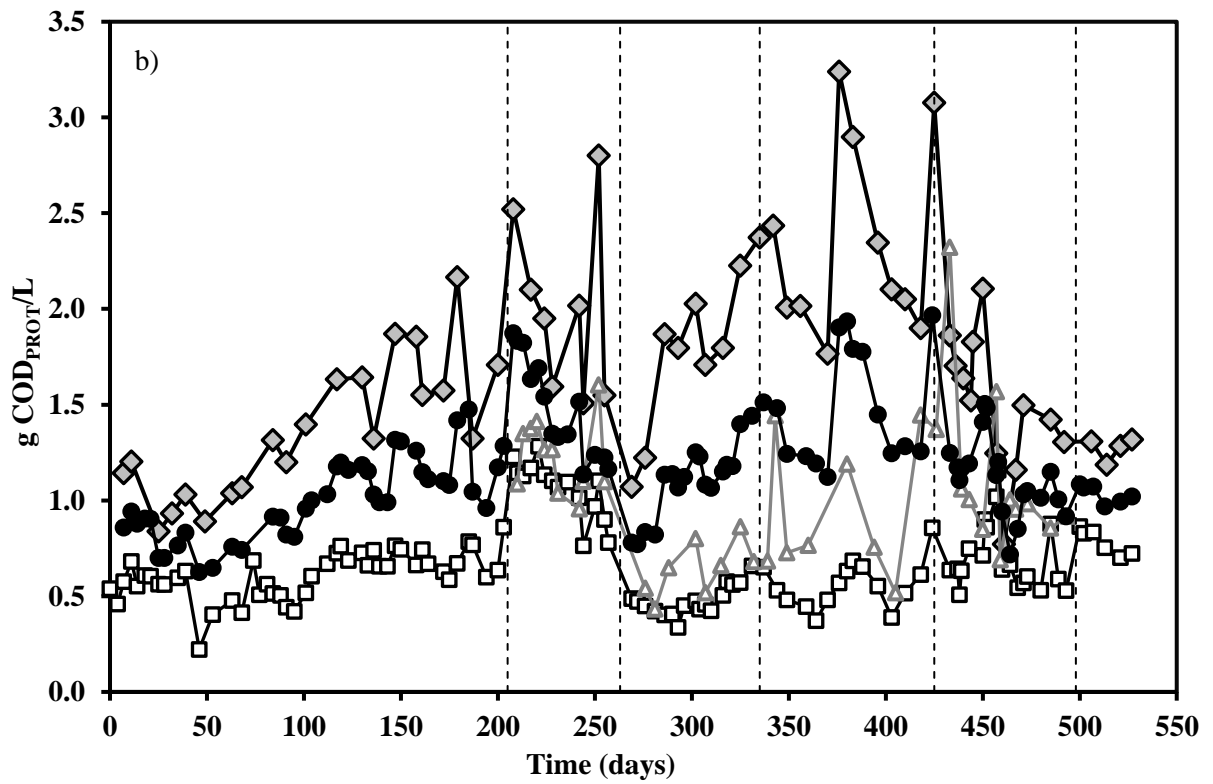


Figure 2

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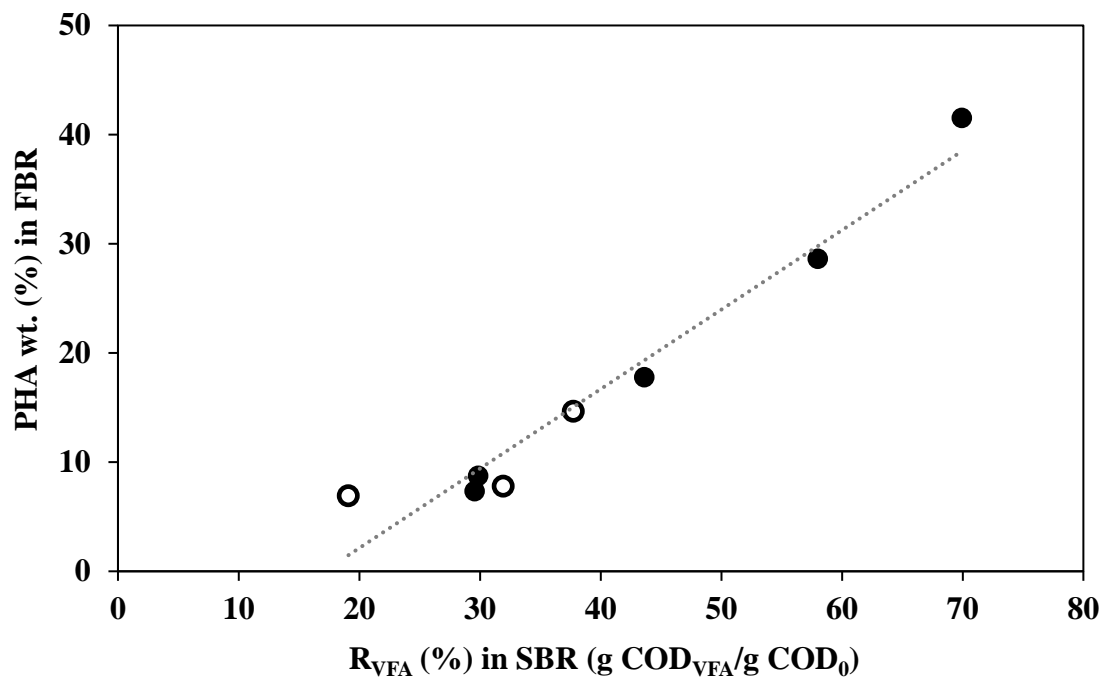
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Figure 3



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Figure 4